

1 Primitive Chain Network Simulations for H-Polymers under Fast Shear

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12 **ABSTRACT**

13 Branchpoint Withdrawal (BPW) has been recognized as one of the important molecular mechanisms
14 for the description of the dynamics of entangled branched polymers under fast flows. However, the
15 relation to the other known molecular mechanisms has not been fully elucidated yet. In this study we
16 performed primitive chain network (i.e., multi-chain slip-link) Brownian simulations for a melt of a
17 well-characterized monodisperse H-polymer, for which the linear viscoelasticity and shear viscosity
18 growth curves at several shear rates are available in the literature. After confirming the consistency of
19 the simulations with the rheological data, we used the simulations to analyze the molecular motion in
20 detail. The results reveal that molecular tumbling occurs in branched polymers just as in linear ones,
21 and that it is accelerated by BPW. Furthermore, BPW not only mitigates backbone stretch, as expected,
22 but also arm stretch. However, because the transient startup viscosity is anyhow dominated by chain
23 stretch dynamics rather than by molecular tumbling, our results rationalize the fact that pom-pom
24 theories successfully ignore tumbling in shear flows.

25
26 **KEYWORDS**

27 Viscoelasticity, molecular simulations, start-up shear, shear thinning.

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33 INTRODUCTION

34 Branchpoint withdrawal (BPW)¹ is one of the established molecular mechanisms for the
35 description of branched polymer dynamics under fast flows. In the tube-theory framework, entangled
36 polymer dynamics is focused on the motion of a test molecule subjected to a tube-shaped constraint,
37 representing the mean field exerted by the surrounding molecules.² For the case of branched polymers,
38 the arms are confined in their own tubes that emanate from the main tube of the backbone, and the
39 reptation motion of the backbone is triggered by arm retraction.³ On top of this thermal, hierarchical
40 relaxation, under fast flows an additional relaxation mechanism takes place: the branchpoint is
41 withdrawn into the backbone tube when the tension in the backbone exceeds the entropic barrier of
42 such improbable conformation.¹ As a consequence, the backbone tension is upper limited, and it is
43 presumably lower than the maximum tension determined by the finite chain extensibility. Such a
44 suppressed extension of the backbone has been observed experimentally.⁴ The molecular constitutive
45 equation based on this BPW idea, the so-called pom-pom constitutive equation,¹ has attained great
46 success for the description of branched polymer rheology under elongational flows. Several modified
47 models have been proposed for better predictions, and/or numerical convenience, in macroscopic flow
48 calculations.⁵⁻⁹

49 Even though BPW is such a significant mechanism, there are a few open questions
50 concerning the relation to the other known, important molecular mechanisms. For example, several
51 years ago, we discussed about competition between BPW and convective constraint release (CCR).¹⁰
52 CCR is a flow-induced increase of the relaxation rate for the reptation motion, due to renewal of
53 topological obstacles associated to the relative convective motion among neighboring molecules.¹¹
54 Although CCR has been unanimously considered an important molecular mechanism in the dynamics
55 of entangled linear polymers under fast flows, to our knowledge CCR has never been implemented
56 into the pom-pom models, differently from the thermal constraint release, which is accounted for
57 through the so-called tube dilation.¹² Because CCR certainly contributes to the relaxation of the
58 backbone, the occurrence of BPW could be suppressed by CCR via the reduction of the backbone
59 tension. Hence, in order to observe the rate of occurrence of these events, we performed multi-chain
60 slip-link Brownian simulations for a pom-pom polymer melt under fast uniaxial elongation, and
61 showed that for such flows BPW overwhelms CCR.¹⁰ This observation rationalizes absence of CCR
62 in the pom-pom models in elongational flows.

63 In this study, we examine the contribution of BPW under fast shear flows, also in relation to
64 the shear-induced molecular tumbling motion. In the original pom-pom paper, Larson and McLeish¹
65 demonstrated that BPW does not play any significant role in shear flows, given that the magnitude of
66 the backbone stretch does not exceed the critical value to overcome the entropic barrier. However,
67 BPW would be activated by the local force balance around the branchpoint even if the entire backbone
68 stretch is not significant. Besides, in shear flows BPW could be affected by the tumbling motion of

69 the molecules. Recent molecular simulations have shown that polymers undergo a quasi-periodic
70 tumbling motion under shear.¹³⁻¹⁵ Although, conceptually, such a flow-induced molecular motion
71 should be included in CCR, Costanzo et al.¹⁶ considered the tumbling motion separately from CCR to
72 explain the stress undershoot at high shear rates. Intuitively, the tumbling motion is expected to occur
73 for branched polymers as well. However, for tumbling to be possible, the network formed among the
74 backbones must be periodically renewed, and BPW is expected to contribute to such a network
75 renewal.

76 We here report on multi-chain slip-link simulations (so-called primitive chain network
77 simulations¹⁷) for a well-characterized monodisperse H-polymer melt, for which the linear
78 viscoelasticity¹⁸ and the stress growth at high shear rates¹⁹ are available in the literature. As previously
79 examined for the other branched polymers,^{10,20-24} the present simulation semi-quantitatively
80 reproduces the linear viscoelasticity. In view of such agreement, we determined the units of time and
81 stress, and we run the simulations under shear with and without BPW. The simulations with BPW
82 reasonably reproduce the experimental data, whereas those without BPW somewhat overestimate the
83 stress. We next analyzed the molecular motion in detail to conclude that BPW helps the tumbling
84 motion of the backbone, in addition to the expected reduction of stretch. Details are reported below.

85

86 MODEL AND SIMULATIONS

87 Multi-chain slip-link simulations were performed with the extension of the model that
88 includes the topology change around the branchpoint for the hierarchical relaxation^{21,22} and BPW.¹⁰
89 As the simulation scheme used here has already been described in those papers, only a summary is
90 given below.

91 In the simulation, entangled branched polymers are replaced by a network whose nodes are
92 either crosslinks (the branchpoints) or slip-links (the entanglements). By assuming that the
93 entanglements are binary, each slip-link connects two chains. Hence, four network strands depart from
94 each slip-link, one (or two at most) of such strands possibly consisting of dangling ends. Of course,
95 each molecule is a well-defined branched path connecting several chain ends. The state variables of
96 the system are the position of dangling ends and of network nodes $\{\mathbf{R}_i\}$, the number of monomers in
97 each network strand or dangling end $\{n_i\}$, the number of strands in each subchain $\{Z_j\}$ (subchains
98 connect either consecutive branchpoints of the backbone or a branchpoint to the chain end of the
99 corresponding arm), and the connectivity matrix of the subchains for each molecule $\{C_k\}$. For $\{\mathbf{R}_i\}$,
100 the dynamics is described by a Langevin-type equation of motion, in which the force balance relates
101 the drag force, the tension force acting in each strand emanating from the node, the osmotic force due
102 to density inhomogeneities, and the random force of thermal motion. The kinetics of $\{n_i\}$ is
103 calculated according to the rate equation that takes account of a force balance like that of the $\{\mathbf{R}_i\}$ -
104 dynamics, here applied to consecutive strands of the molecule across a slip-link. $\{Z_j\}$ changes with

105 time due to the creation or destruction of slip-links at the chain ends. Indeed, when the number of
106 monomers on a dangling end becomes smaller than a threshold value because of the kinetics
107 mentioned above, the associated slip-link is removed, and consequently the two strands of each of the
108 two chains merge into one. Conversely, a new slip-link is created when the number of monomers in
109 the chain end exceeds a maximum value, and the companion of the chain end is a strand chosen
110 randomly from the surroundings. Because no chemical reaction is considered, $\{C_k\}$ is kept
111 unchanged throughout the simulations.

112 The dynamics so far described is enough for linear polymers. For branched ones, additional
113 rules governing topological changes around the branchpoints are necessary. One of such rules is the
114 hierarchical relaxation, according to which reptation of the backbone is allowed when the branching
115 arms relax.³ In our implementation, we allow the branchpoint to hop across the next slip-link when no
116 slip-link happen to exist on the branching arms emanating from the branchpoint.²¹ Following the
117 previous study,¹⁰ we refer to this topological change as branchpoint reptation (BPR). A different
118 possibility is the previously mentioned BPW, when we “suck” the branchpoint and the arms into the
119 slip-link next to the branchpoint when the local tension force in the backbone strand emanating from
120 the branchpoint exceeds the sum of the tension forces of the arm strands.¹⁰

121 Although finite chain extensibility and stretch/orientation-induced reduction of friction play
122 some role in elongational flows as reported earlier,^{25,26} they are not considered in this study because
123 we focus on the behavior under shear, where they are expected to be only marginally relevant.

124 In this study, the simulations were performed for a melt of monodisperse H-shaped
125 polystyrene molecules, known by the code H3A1A.¹⁸ The molar mass of the arm and of the backbone
126 are $M_a = 132\text{k}$ and $M_b = 123\text{k}$, respectively. According to the conversion factor for the molar mass
127 for polystyrene melts earlier determined as $M_0 = 11\text{k}$,^{27,28} the average number of the network strands
128 under equilibrium for the arm and the backbone are $Z_{a0} = 12$, and $Z_{b0} = 11$, respectively.

129 The units of length, energy, and time used in the simulations are, respectively, the
130 equilibrium strand root-mean-square length a , the thermal energy $k_B T$, and the diffusion time of the
131 strand $\tau_0 \equiv \zeta a^2 / 6k_B T$, where ζ is the friction coefficient of a chain segment with molar mass M_0 .
132 The simulations were performed with a periodic boundary condition, for which the box volume was
133 fixed at 10^3 . Twelve independent quiescent simulations starting from different initial configurations
134 were run for a sufficiently long period of time, which is more than ten times longer than the longest
135 relaxation time of the system. For the recorded stress fluctuating with time, we disregarded the former
136 half to eliminate possible artifacts arising from the initial state. The linear relaxation modulus was then
137 obtained via the Green-Kubo formula for the remaining latter half. The relaxation modulus was then
138 converted to the complex moduli through fitting to a multi-mode Maxwell function with the help of
139 the REPTATE code.²⁹ To the equilibrium configurations, as attained in the quiescent simulations, shear
140 flows were applied via a SLLOD-like method, in which a small affine deformation was introduced at

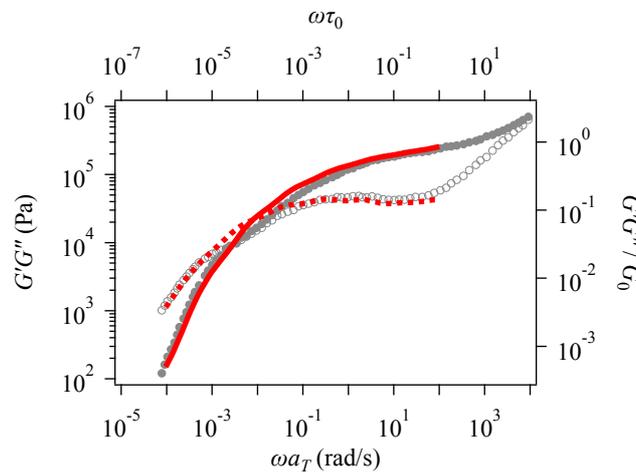
141 each integration time step. The Lees-Edwards boundary conditions were also employed.

142

143 RESULTS

144 Figure 1 shows linear viscoelasticity simulation results, compared to the experimental
145 data.¹⁸ With the conversion factors for time and modulus that are determined as $\tau_0 = 0.01\text{s}$ and $G_0 =$
146 0.3MPa , the simulation (red curves) reasonably reproduces the experimental results (symbols). To be
147 fair, we note that around the crossover of the G' and G'' curves the simulation slightly overestimates
148 the modulus. Because this tendency was also observed for the other H-polystyrenes earlier examined,²⁴
149 the discrepancy reasonably implies some (minor) flaw in the model. Not knowing better, we accepted
150 the predicted linear viscoelastic response given in Fig. 1 (with the corresponding equilibrium
151 configurations), and we proceeded with the simulations of shear startup from such initial states.

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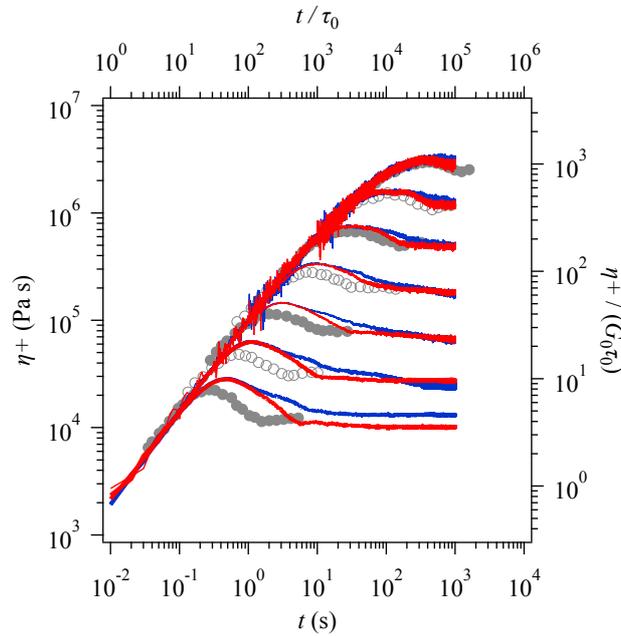
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154 **Figure 1** Linear viscoelasticity of H polystyrene melt. Red curves are simulation results, and filled
155 and unfilled circles indicate experimental data¹⁸ at 169.5°C . Solid curve and filled symbols are G' , and
156 dotted curve and unfilled symbols are G'' .

157

158 Figure 2 shows the viscosity growth under fast shear calculated with the time and modulus
159 conversion factors mentioned above. The simulation results are in good agreement with the
160 experimental data¹⁹ if the shear rate is relatively low. As the shear rate increases, the simulation
161 deviates from the data. Specifically, for the viscosity overshoot, the peak appears somewhat later, and
162 the viscosity grows higher. The discrepancy in the viscosity overshoot might be related to the
163 inconsistency in the linear viscoelasticity. Nevertheless, the steady-state viscosity is semi-
164 quantitatively reproduced. Although these features are present both with and without BPW, the
165 simulation with BPW (red curves) better captures the experiment than that without BPW (blue curves).
166 In particular, the simulation without BPW shows a delayed mitigation of the viscosity after the
167 overshoot, *i.e.*, moving towards the steady state. McLeish et al.³⁰ mentioned that, in the pom-pom

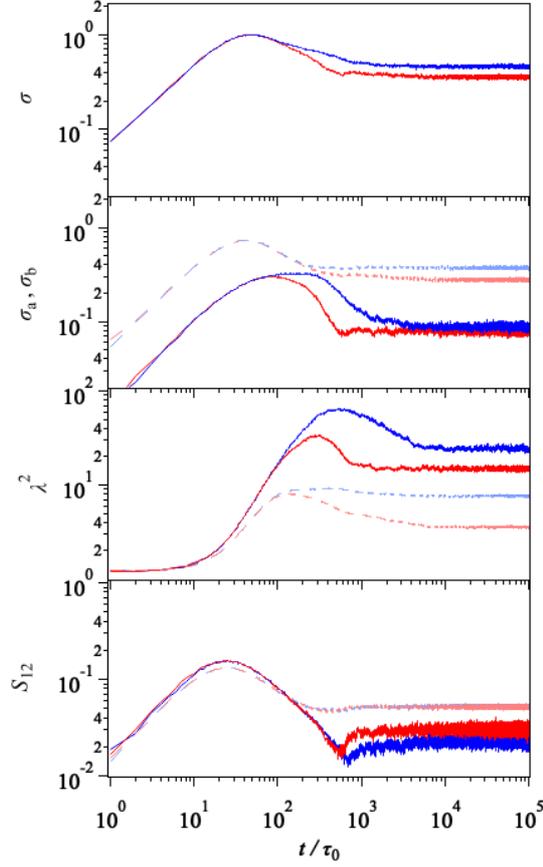
168 constitutive equation, BPW affects the magnitude of the overshoot, but we do not observe such an
 169 effect.
 170



171
 172 **Figure 2** Viscosity growth of H polystyrene melt under fast shear. Shear rate are 0.01, 0.032, 0.1, 0.32,
 173 1, 3.2, and 10 s^{-1} , from top to bottom. Red and blue curves are simulation results with and without
 174 BPW, respectively, and both filled or unfilled circles indicate experimental data¹⁹ at 169.5°C.
 175

176 To see the role of BPW in detail, we analyzed stress, strand stretch, and strand orientation
 177 for the arm and backbone subchains separately. Results are shown in Fig. 3 for the case of a shear rate
 178 of 10 s^{-1} . As seen in the top panel (as well as in Fig. 2), BPW accelerates relaxation of the stress after
 179 the maximum. The decomposed stress shown in the second panel of Fig. 3 reveals that such
 180 acceleration comes from the backbone contribution (solid curves). Indeed, in the simulation without
 181 BPW (blue curves), relaxation of the backbone stress is delayed. For the arms (broken curves), the
 182 transient stress is virtually insensitive to BPW. Moreover, BPW also lowers the steady-state value.
 183 These effects of BPW appear to be due to reduction of the strand stretch (third panel). BPW contributes
 184 to relief of the stretch for both backbone and arms, and it also lowers the steady state values. Reduction
 185 of the backbone stretch is in harmony with the original idea of BPW, whereas reduction of the arm
 186 stretch goes beyond the classical tube modeling. The difference in the arm stretch with and without
 187 BPW reflects the renewal rate of the entanglement network. As discussed later, BPW accelerates
 188 molecular tumbling, which goes together with a renewal of the entanglement network surrounding the
 189 tumbling chain. Because the entanglements between backbones and arms are included in such a
 190 renewed network, BPW mitigates arm stretch as well as the backbone stretch. The segment orientation

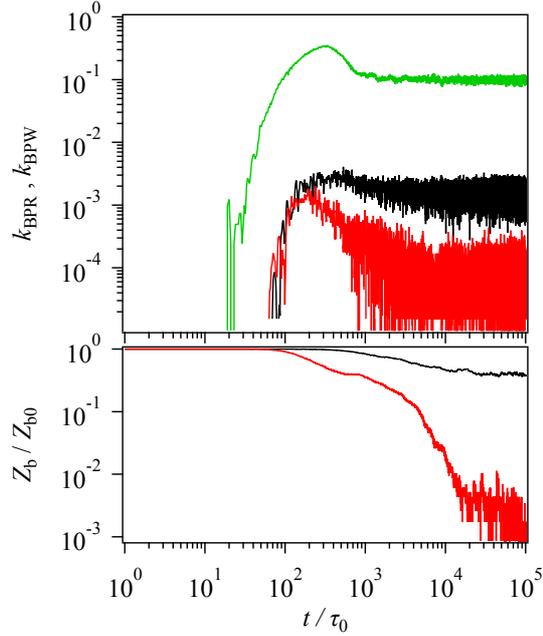
191 (bottom panel) is not strongly affected by BPW, apart from a weak over-orientation seen in the
 192 backbone subchain (blue solid curve). The backbone strand orientation shows a clear undershoot that
 193 reflects a rotating motion of the backbone, as shown later.



194
 195 **Figure 3** Stress during shear startup for the entire system (top panel), contribution to stress from arms
 196 and backbones (2nd panel), squared strand stretch (3rd panel), and strand orientation (bottom panel) at
 197 $\dot{\gamma} = 10 \text{ s}^{-1}$. Red and blue curves are from the simulations with and without BPW, respectively. Solid
 198 and dotted curves indicate results for backbones and arms, respectively.

199
 200 Figure 4 (top panel) shows the rate of BPW and BPR events per molecule, k_{BPW} and k_{BPR} ,
 201 at the shear rate of 10 s^{-1} . k_{BPW} (green curve) steeply grows in a short time, during which the local
 202 tension becomes sufficiently strong due to the deformation. As a result of BPW, the number of
 203 entanglements in the backbone decreases with time (as shown by the red curve in the bottom panel),
 204 which in its turn makes k_{BPW} to go through an overshoot. Because the peak position of k_{BPW}
 205 coincides with that for the strand stretch (see 3rd panel in Fig. 3), we may conclude that relief of the
 206 stretch is indeed induced by BPW. k_{BPR} is shown in Fig. 4 by red and black curves for the simulations
 207 with and without BPW. k_{BPR} is affected by the convection because the entanglements formed
 208 between arms and between arm and backbone are removed by the translational motion of the

209 molecules, i.e., by CCR. However, even with such a flow-induced enhancement, k_{BPR} is not
 210 comparable to k_{BPW} at this specific shear rate. This result means that BPW is the dominating
 211 mechanism for the disentanglement of the network of backbones, and it confirms the fact that in pom-
 212 pom theories CCR can be ignored. The rate k_{BPR} comes out smaller in the simulation with BPW (red
 213 curve) than that without BPW (black curve) because BPW dominates in removing entanglements.
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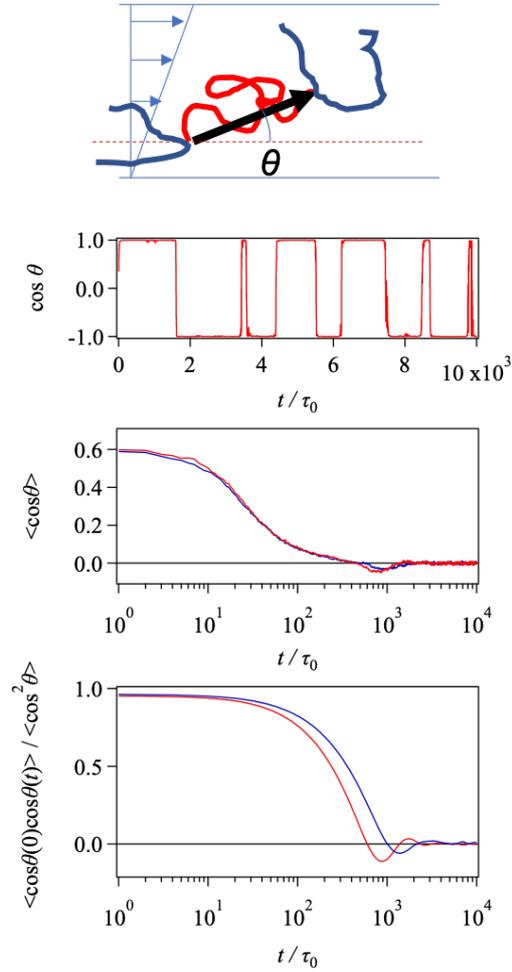


215
 216 **Figure 4 (Top)** Time development of the rate of BPW and BPR events per molecule at $\dot{\gamma} = 10 \text{ s}^{-1}$. For
 217 the simulation with BPW, the rate of BPW and BPR is shown by green and red curves. For the
 218 simulation without BPW, the BPR rate is shown by the black curve. (Bottom) Number of backbone
 219 entanglements (normalized to its equilibrium value) as a function of time. Red and black curves show
 220 the results of simulations with and without BPW, respectively.
 221

222 The bottom panel in Fig. 4 shows the time development of the number Z_b of backbone
 223 entanglements at $\dot{\gamma} = 10 \text{ s}^{-1}$, normalized to its equilibrium value Z_{b0} . In the simulation with BPW (red
 224 curve) the backbone entanglements are efficiently removed, and their number virtually goes down to
 225 zero. Decrease of the backbone entanglements reflects the growth of the BPW rate shown in the top
 226 panel. In the simulation without BPW there remain some of the backbone entanglements, which are
 227 enough to form a network. This network induces a larger strand stretch, as shown in Fig. 3.

228 To evaluate the effect of BPW on the rotation of the molecules, we define the rotation angle
 229 θ of the backbone in the following way. The pseudo-vector connecting the branchpoints of the H-
 230 polymer is projected onto the plane formed by the shear and gradient directions. We then call θ the
 231 angle formed by such projection with the shear direction (see top panel in Fig. 5). Although θ is

232 defined in the whole range $]-\pi, \pi]$, at the flow startup ($t = 0$) this angle may be restricted to the
233 range $-\pi/2 < \theta \leq \pi/2$ so that $\cos \theta \geq 0$. The second panel in Fig. 5 shows an example of the
234 time development of $\cos \theta$ at $\dot{\gamma} = 10 \text{ s}^{-1}$. As reported for linear polymers,³¹ $\cos \theta$ exhibits a sort of
235 flip-flop behavior that reflects the molecule rotation under shear. Figure 5 (third panel) is the ensemble
236 average of $\cos \theta(t)$ obtained from 100 chains. Because of the random orientations at the initial
237 condition (i.e. all θ values are equally probable), $\langle \cos \theta(t = 0) \rangle = 2/\pi$. Next, because of flow,
238 $\langle \cos \theta(t) \rangle$ decays to zero. However, around $t/\tau_0 \sim 1000$, a negative undershoot is found, which
239 clearly indicates a coherent rotation of the different backbones. This feature is also seen in the
240 backbone orientation (going back to the bottom panel of Fig. 3). We further note that the undershoot
241 occurs slightly earlier in the simulation with BPW than in that without BPW. Finally, the bottom panel
242 of Fig. 5 shows the auto-correlation function of $\cos \theta(t)$ in the steady state. Here, oscillations around
243 zero start at a time roughly corresponding to that of the undershoot in $\langle \cos \theta(t) \rangle$, although they do
244 not imply coherence among the molecules. We can also infer that BPW augments rotation of the
245 molecule (red vs. blue curve), and the faster rotation causes a more rapid relaxation of the stress after
246 the overshoot via relief of the stretch.
247



248

249 **Figure 5** Schematic representation of the rotation angle θ of the backbone (top). Typical example of
 250 the time development of $\cos \theta$ after the flow startup at $\dot{\gamma} = 10 \text{ s}^{-1}$ (second top). Ensemble average
 251 of $\cos \theta$ (second bottom). Autocorrelation function of $\cos \theta$ in the steady state (bottom). Red and
 252 blue curves are the results from the simulations with and without BPW, respectively.

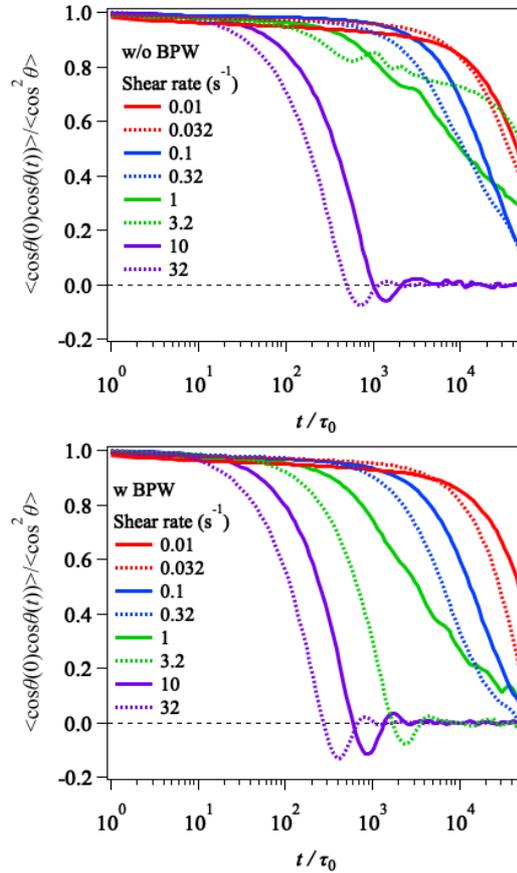
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254 Figure 6 shows the effect of the shear rate on the autocorrelation function of $\cos \theta(t)$. The
 255 characteristic time for the decay decreases with increasing the shear rate, and the dumped-oscillatory
 256 behavior is observed only at high shear rates. These basic features, which are consistent with the earlier
 257 report for MD simulations of linear polymers,¹⁴ can be seen for both simulations, with and without
 258 BPW.

259

The Weissenberg number to induce tumbling comes out much higher for the branched
 260 polymer here examined than for the linear polyethylene of Nafar-Sefiddashti et al.¹⁴ Indeed, the critical
 261 Weissenberg number (beyond which tumbling occurs) reported by them is around 100, whereas it is
 262 more than 1000 in this study. This suggests that the branched structure tends to suppress tumbling.
 263 Concerning the effect of BPW, it accelerates the decay of correlation, and it induces the dumped-

264 oscillatory behavior at a shear rate smaller than that for the case without BPW. These observations
 265 clearly demonstrate that BPW significantly affects molecular tumbling.
 266



267
 268 **Figure 6** Autocorrelation of $\cos \theta (t)$ at several shear rates, with and without BPW (bottom and top
 269 panels, respectively).

270
 271

272 **DISCUSSION AND CONCLUSIONS**

273 Costanzo et al¹⁶ proposed a constitutive equation that accounts for the effect of tumbling under shear
 274 to reproduce the stress undershoot following the overshoot. Specifically, they introduced dumped
 275 oscillations to the chain strand orientation assuming that tumbling coherence initiated by shear
 276 vanishes with time. This idea is consistent with our results shown in Figs 3 and 5, in which we observe
 277 some coherence in the rotation of the backbone. Rotation of the backbone also appears as a dumped
 278 oscillation in the autocorrelation function of the backbone orientation. However, no stress undershoot
 279 is observed because of the contribution of stretch. Indeed, the two bottom panels in Fig. 3 show that
 280 the stretch overshoot occurs later than that of the orientation. Consequently, the undershoot of
 281 orientation overlaps with the overshoot of stretch, thus cancelling a possible stress undershoot. Besides,

282 for the H-polymer here examined the total stress is dominated by the contribution of the arms, for
283 which the undershoot of the segment orientation is faint. According to these results, we may conclude
284 that the theory proposed by Costanzo et al¹⁶ does not apply to the H-polymer here examined, and
285 would perhaps be applicable to branched polymers with a different structure.

286 In conclusion, we investigated the effect of BPW on the motion of branched polymers
287 undergoing fast shear flows using primitive-chain-network simulations for a polystyrene melt of H
288 molecules. The simulation reasonably reproduces the linear viscoelasticity and the shear viscosity
289 growth curve reported in the literature. Based on this agreement with the rheological data, we analyzed
290 the molecular motion in detail. The results demonstrate that BPW reduces the backbone stretch as
291 expected, while it also contributes (unexpectedly) to mitigate the arm stretch. Due to reduction in the
292 stretch, BPW yields better prediction for the viscosity growth under fast shear. Furthermore, BPW
293 accelerates molecular tumbling at high shear rates, although tumbling effects do not explicitly appear
294 in the viscosity growth curve (no undershoot). The rate of BPW is significantly larger than the rate of
295 convection-induced disentanglement. Consequently, it so appears that the reduced chain stretch
296 induced by BPW overwhelms the other stress-determining molecular mechanisms in shear startup.
297 The dominance of BPW is in harmony with our earlier study on a pom-pom polystyrene melt under
298 uniaxial extension, and it also supports pom-pom theories, in which CCR and molecular tumbling are
299 not considered.

300

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