

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32

**Applicability of Dynamic Mode Decomposition to Estimate Fundamental Mode  
Component of Prompt Neutron Decay Constant from Experimental Data**

Fuga Nishioka<sup>a\*</sup>, Tomohiro Endo<sup>a</sup>, Akio Yamamoto<sup>a</sup>,  
Masao Yamanaka<sup>b†</sup>, Cheol Ho Pyeon<sup>b</sup>

<sup>a</sup>*Nagoya University, Graduate School of Engineering, Department of Applied Energy,  
Nagoya, Japan*

<sup>b</sup>*Kyoto University, Institute for Integrated Radiation and Nuclear Science, Osaka,  
Japan*

Corresponding author: Fuga Nishioka

\*E-mail: f-nishioka@fermi.energy.nagoya-u.ac.jp

Address: Nagoya University, Furo-cho, Chikusa-ku, Nagoya, Japan, 464-8603

Tel, Fax: +81-52-789-3775, +81-52-789-3608

Number of Pages: 19

Number of Tables: 2

Number of Figures: 6

† Present affiliation: *Nuclear Engineering, Ltd., Osaka, Japan*

33 **ABSTRACT**

34

35 To robustly estimate the fundamental mode component of prompt neutron decay  
36 constant  $\alpha$  in a subcritical system, dynamic mode decomposition (DMD) is applied to  
37 time-series data obtained by the pulsed-neutron source (PNS) and Rossi- $\alpha$  methods. For  
38 the statistical uncertainty quantification of  $\alpha$  by DMD, randomly sampled virtual data  
39 are used for the DMD procedure. The applicability of DMD is demonstrated by  
40 analyzing the experimental results by the PNS and Rossi- $\alpha$  methods, which are  
41 performed at the Kyoto University Critical Assembly (KUCA). When applying the  
42 DMD to the PNS and Rossi- $\alpha$  experimental data, a constant signal was added to the  
43 experimental data to remove the background constant component. The application  
44 results indicate that DMD enables one to robustly estimate the fundamental mode  
45 component of  $\alpha$  in the PNS and Rossi- $\alpha$  methods.

46

47 **KEYWORDS:** prompt neutron decay constant, dynamic mode decomposition,  
48 fundamental mode component, pulsed-neutron source method, Rossi- $\alpha$  method

49

## 50 I. INTRODUCTION

51 The prompt neutron decay constant  $\alpha$  is a time constant that represents the  
52 exponential decay of the number of prompt neutrons in a subcritical system. The  
53 experimental value of the fundamental mode component of  $\alpha$  is useful for estimating the  
54 subcriticality of the measurement system and reducing nuclear data-induced  
55 uncertainties in numerical results using data assimilation [1]. The fundamental mode  
56 component shows the slowest decay among those of higher mode components obtained  
57 by the time-dependent prompt neutron transport equation. Therefore, when sufficient  
58 time has elapsed after a source neutron is generated, the fundamental mode component  
59 becomes the most dominant component of the neutron flux in the system.

60 The pulsed neutron source (PNS) method [2] and the Rossi- $\alpha$  method [3] can be  
61 applied to obtain the  $\alpha$  value experimentally. In the PNS method, the time variation of  
62 neutron count rates in the subcritical system is measured by periodically injecting  
63 pulsed neutrons into the subcritical system. After pulsed neutrons are injected into the  
64 subcritical system, the neutron count rates temporarily increase due to the neutron  
65 transport and the fission chain reaction caused by the pulsed neutrons. Subsequently,  
66 since the fission chain reaction terminates in the subcritical system, the neutron count  
67 rates exponentially decrease by a system-specific decay constant. The system-specific  
68 decay constant corresponds to  $\alpha$ . By contrast, in the Rossi- $\alpha$  method, the reactor noise  
69 signals in the subcritical system are measured to obtain a histogram of the neutron-  
70 detection-time intervals. The histogram of the neutron-detection-time intervals  
71 corresponds to the time variation of the probability that a neutron pair belonging to the  
72 same fission chain system is detected. The probability also decreases exponentially by  
73 the prompt neutron decay constant  $\alpha$ . Generally, the value of  $\alpha$  is estimated by the least-  
74 squares fitting method using an exponential function to the measured time-series data of  
75 the PNS or Rossi- $\alpha$  method.

76 The problem of the least-squares fitting method is that the estimated  $\alpha$  contains  
77 a systematic error derived from the higher mode components because a precise  
78 extraction of only the fundamental mode component is difficult. To reduce the influence  
79 of higher mode components, the time-series data obtained by the PNS or Rossi- $\alpha$   
80 method within a masking time interval are excluded in the conventional least-squares  
81 fitting. In other words, the estimated value of  $\alpha$  depends on the masking time. To  
82 address this issue, Katano proposed linear combination method [4–6]. In this method,

83 the time-series data acquired using multiple detectors are summed with the weighting  
84 coefficients, to be expressed as a single exponential decay as much as possible.  
85 However, not only the value of  $\alpha$  but also the weighting coefficients should be  
86 determined by the nonlinear least-squares fitting. Hence, the initial values of these  
87 fitting parameters must be assigned appropriately to estimate the fundamental mode  
88 component of  $\alpha$ , i.e., there is an issue to set the initial values of these fitting parameters  
89 automatically.

90 To overcome this issue, we aim to develop another method that can robustly  
91 estimate the fundamental mode component of  $\alpha$  without requiring any initial values in  
92 the conventional fitting process. For this purpose, this study focused on dynamic mode  
93 decomposition (DMD). DMD is a data-driven method that can extract the spatio-  
94 temporal structure of a system from time-series data obtained from experiments or  
95 numerical simulations [7]. Recently, DMD has been investigated in the field of reactor  
96 physics, e.g., to construct the reduced order models of kinetic properties in subcritical  
97 systems [8]. In DMD, the time constant for each mode can be obtained by decomposing  
98 the time-series data into a summation of exponential modes. Since the experimental  
99 results obtained by the PNS and Rossi- $\alpha$  methods can also be expressed by the  
100 summation of exponential functions, the applicability of DMD to both methods is  
101 expected. Furthermore, unlike conventional fitting and linear combination methods,  
102 DMD does not require any initial values, i.e., the fundamental mode component of  $\alpha$   
103 can be uniquely determined from the time constant obtained by applying DMD. In this  
104 study, the applicability of DMD for extracting the fundamental mode component of  $\alpha$   
105 from actual experimental results by the PNS and Rossi- $\alpha$  methods was investigated.

106 The remainder of this paper is organized as follows. In Section II, the theoretical  
107 formulas of the PNS and Rossi- $\alpha$  methods are briefly explained. Subsequently, the  
108 theory of DMD is presented, followed by a procedure to estimate the statistical  
109 uncertainty of  $\alpha$  by DMD using randomly sampled virtual data. Section III describes the  
110 PNS and Rossi- $\alpha$  experiments performed at the Kyoto University Critical Assembly  
111 (KUCA) and presents the application results of DMD for each experiment. Finally,  
112 concluding remarks are presented in Section IV.

113

114 **II. THEORY**

115 **II.A. Pulsed-Neutron Source and Rossi- $\alpha$  Methods**

116 In the PNS method, pulsed neutrons are periodically injected into the subcritical  
 117 system, and then the time variation in the neutron count rate  $C(t)$  is measured. The  
 118 prompt neutron decay constant  $\alpha$  is estimated by analyzing the exponential time  
 119 variation of  $C(t)$ .

120 The theoretical formula for the neutron flux after pulsed neutrons are injected  
 121 into a subcritical system is explained briefly below. First, let us define Green's function  
 122  $G(\vec{r}, E, \vec{\Omega}, t | \vec{r}_0, E_0, \vec{\Omega}_0, t_0)$  as the neutron flux at  $(\vec{r}, E, \vec{\Omega}, t)$  after injecting one neutron  
 123 into the system at  $(\vec{r}_0, E_0, \vec{\Omega}_0, t_0)$ . Here,  $\vec{r}$ ,  $E$ ,  $\vec{\Omega}$ , and  $t$  represent the position, neutron  
 124 energy, neutron flight direction, and time variables, respectively; the subscript 0  
 125 indicates the index for neutron injection. By focusing on the time domain where the  
 126 decay of prompt neutron component is dominant, the Green's function  
 127  $G(\vec{r}, E, \vec{\Omega}, t | \vec{r}_0, E_0, \vec{\Omega}_0, t_0)$  can be expanded using the  $\alpha$ -eigenfunction as follows [9]:

$$G(\vec{r}, E, \vec{\Omega}, t | \vec{r}_0, E_0, \vec{\Omega}_0, t_0) = \sum_{n=0}^{\infty} \psi_n(\vec{r}, E, \vec{\Omega}) \psi_n^\dagger(\vec{r}_0, E_0, \vec{\Omega}_0) e^{-\alpha_n(t-t_0)}, \quad (1)$$

128 where  $\psi_n$  and  $\psi_n^\dagger$  represent the forward and adjoint eigenfunctions, respectively. These  
 129 eigenfunctions satisfy the following forward and adjoint prompt- $\alpha$  eigenvalue equations  
 130 using the conventional nomenclature in the reactor physics:

$$\mathbf{B}\psi_n(\vec{r}, E, \vec{\Omega}) = \frac{\alpha_n}{v(E)} \psi_n(\vec{r}, E, \vec{\Omega}), \quad (2)$$

$$\mathbf{B}^\dagger \psi_n^\dagger(\vec{r}, E, \vec{\Omega}) = \frac{\alpha_n}{v(E)} \psi_n^\dagger(\vec{r}, E, \vec{\Omega}), \quad (3)$$

131 where vacuum conditions are assumed for  $\psi_n$  and  $\psi_n^\dagger$  at the outer boundary conditions;  
 132  $\mathbf{B}$  and  $\mathbf{B}^\dagger$  are the forward and adjoint Boltzmann operators, respectively, defined as  
 133 follows:

$$\begin{aligned} \mathbf{B} \equiv & \vec{\Omega} \cdot \nabla + \Sigma_t(\vec{r}, E) - \int_0^\infty dE' \int_{4\pi} d\Omega' \Sigma_s(\vec{r}, E' \rightarrow E, \vec{\Omega}' \rightarrow \vec{\Omega}) \\ & - \frac{\chi_p(\vec{r}, E)}{4\pi} \int_0^\infty dE' \int_{4\pi} d\Omega' v_p \Sigma_f(\vec{r}, E'), \end{aligned} \quad (4)$$

$$\mathbf{B}^\dagger \equiv -\vec{\Omega} \cdot \nabla + \Sigma_t(\vec{r}, E) - \int_0^\infty dE' \int_{4\pi} d\Omega' \Sigma_s(\vec{r}, E \rightarrow E', \vec{\Omega} \rightarrow \vec{\Omega}') - \nu_p \Sigma_f(\vec{r}, E) \int_0^\infty dE' \int_{4\pi} d\Omega' \frac{\chi_p(\vec{r}, E')}{4\pi}. \quad (5)$$

134 To derive the theoretical formula of the PNS method, let us assume that delta-functional  
 135 neutrons  $q_{\text{PNS}}$  are repeatedly injected with a constant period  $T_0$  at time  $t = -iT_0$  ( $i =$   
 136  $0, 1, 2, \dots$ ). In the steady-state after sufficient time from the start of pulsed neutron  
 137 injection, an approximately constant background neutron source  $q_{\text{BG}}$  exists in the  
 138 system because of the inherent neutron source (e.g., spontaneous fission and  $(\alpha, n)$   
 139 reaction) in the nuclear fuel and the decay of delayed neutron precursors. Hence, the  
 140 total neutron source  $q(\vec{r}, E, \vec{\Omega}, t)$  in the system can be expressed as follows:

$$q(\vec{r}, E, \vec{\Omega}, t) = q_{\text{PNS}}(\vec{r}, E, \vec{\Omega}) \left( \sum_{i=0}^{\infty} \delta(t - iT_0) \right) + q_{\text{BG}}(\vec{r}, E, \vec{\Omega}). \quad (6)$$

141 Based on Eqs. (1) and (6), the time variation of the neutron flux  $\psi(\vec{r}, E, \vec{\Omega}, t)$  due to the  
 142 PNS can be derived by integrating the product of Green's function  
 143  $G(\vec{r}, E, \vec{\Omega}, t | \vec{r}_0, E_0, \vec{\Omega}_0, t_0)$  and  $q(\vec{r}, E, \vec{\Omega}, t)$  as follows:

$$\begin{aligned} & \psi(\vec{r}, E, \vec{\Omega}, t) \\ &= \int_V dV_0 \int_0^\infty dE_0 \int_{4\pi} d\Omega_0 \int_{-\infty}^t dt_0 q(\vec{r}_0, E_0, \vec{\Omega}_0, t_0) G(\vec{r}, E, \vec{\Omega}, t | \vec{r}_0, E_0, \vec{\Omega}_0, t_0) \\ &= \sum_{n=0}^{\infty} F_n(\vec{r}, E, \vec{\Omega}) e^{-\alpha_n t} + F_{\text{BG}}(\vec{r}, E, \vec{\Omega}), \end{aligned} \quad (7)$$

144 where  $F_n$  and  $F_{\text{BG}}$  represent the  $n$ 'th order expansion coefficient and the background  
 145 component, respectively. Finally, the time variation of the neutron count rate  $C(t)$  in the  
 146 PNS method can be derived by integrating the product of the macroscopic detection  
 147 cross section  $\Sigma_d$  and the neutron flux  $\psi(\vec{r}, E, \vec{\Omega}, t)$  over the total phase space:

$$C(t) = \langle \Sigma_d \psi \rangle = \sum_{n=0}^{\infty} C_n e^{-\alpha_n t} + C_{\text{BG}}, \quad (8)$$

148 where

149  $\langle \rangle$  = total integral over the total phase space

150  $C_n$  =  $n$ 'th order expansion coefficient

151  $C_{\text{BG}}$  = constant background component.

152 As shown in Eq. (8), the theoretical formula for the neutron count rate  $C(t)$  in  
 153 the PNS method can be expressed by the sum of the exponential higher mode  
 154 components and the constant component [5,6].

155 By contrast, the Rossi- $\alpha$  method is one of the reactor noise analysis methods.  
 156 First, the reactor noise (i.e., time-series data of neutron-detection time) in the subcritical  
 157 system in steady-state condition is measured. Subsequently, the histogram  $P(\tau)$  of the  
 158 neutron-detection-time interval  $\tau$  is obtained by analyzing two detection time points.  
 159 Namely, the time interval  $\tau$  is calculated for each combination of all neutron pairs  
 160 detected within the measurement time, and the histogram  $P(\tau)$  is counted to estimate  
 161 the prompt neutron decay constant  $\alpha$ .

162 The theoretical formula for the histogram  $P(\tau)$  is briefly explained below. Let us  
 163 consider a subcritical system in which the steady-state is maintained by an external  
 164 neutron source. Based on the heuristic method with Green's function expressed in Eq.  
 165 (1) [9,10], the theoretical formula for  $P(\tau)$  can be derived from the  $\alpha$ -eigenfunction  
 166 expansion as follows:

$$P(\tau) = \sum_{n=0}^{\infty} P_n e^{-\alpha_n \tau} + P_u, \quad (9)$$

167 where

168  $P_n = n$ 'th order expansion coefficient

169  $P_u =$  uncorrelated term representing the frequency due to independent neutron  
 170 pairs that do not belong to the same fission chain.

171 As shown in the experimental results of the Rossi- $\alpha$  method in Section III.C.,  
 172 according to the experimental condition, the uncorrelated term  $P_u$  in Eq. (9) can be  
 173 regarded as an almost constant term. In such a case, as in the same manner as the PNS  
 174 method, the theoretical formula for the histogram  $P(\tau)$  in the Rossi- $\alpha$  method can be  
 175 also expressed by the sum of the exponential higher mode components and the constant  
 176 component.

177

## 178 **II.B. Dynamic Mode Decomposition**

179 Let us consider that neutrons are successively counted by  $n$  time steps of time  
 180 interval  $\Delta t$  using  $m$  neutron detectors in the PNS method. Alternatively, in the Rossi- $\alpha$   
 181 method, let us consider that the frequency of the neutron-detection-time interval  $\tau$  is  
 182 measured by  $n$  bins of time interval  $\Delta \tau$  using  $m$  neutron detectors. The discrete time-

183 series data of the PNS or Rossi- $\alpha$  measurement are arranged into an  $m \times n$  matrix  $\mathbf{X}$ ,  
 184 where  $m < n$ . By taking the  $i$ 'th through  $j$ 'th time-series data from the original matrix  
 185  $\mathbf{X}$ , a slicing matrix  $\mathbf{X}_{i,j}$  of size  $m \times (j - i + 1)$  is constructed. Based on two slicing  
 186 matrices  $\mathbf{X}_{1:n-1}$  and  $\mathbf{X}_{2:n}$ , the time evolution matrix  $\mathbf{A}$  in the DMD satisfies the  
 187 following equation [7]:

$$\mathbf{A}\mathbf{X}_{1:n-1} \approx \mathbf{X}_{2:n}. \quad (10)$$

188 For Eq. (10), it is assumed that the time variation of the time-series data is exponential.  
 189 The time evolution matrix  $\mathbf{A}$  transforms each time-step data into the next time-step data.  
 190 In the DMD, the time evolution matrix  $\mathbf{A}$  can be estimated from the time-series data  
 191 only.

192 The procedure to calculate the time evolution matrix  $\mathbf{A}$  is briefly explained  
 193 below. First,  $\mathbf{X}_{1:n-1}$  is decomposed into three matrices using singular value  
 194 decomposition as follows:

$$\mathbf{X}_{1:n-1} = \mathbf{U}\mathbf{\Sigma}\mathbf{V}^*, \quad (11)$$

195 where

196 matrix  $\mathbf{U} = m \times m$  unitary matrix

197 matrix  $\mathbf{\Sigma} = m \times m$  diagonal matrix with diagonal elements corresponding  
 198 to singular values

199 matrix  $\mathbf{V} = (n - 1) \times m$  unitary matrix

200 superscript \* = denotes a complex conjugate transposition.

201 Using Eq. (11), the pseudo-inverse matrix  $\mathbf{X}_{1:n-1}^+$  can be obtained as follows:

$$\mathbf{X}_{1:n-1}^+ = \mathbf{V}\mathbf{\Sigma}^{-1}\mathbf{U}^*, \quad (12)$$

202 where superscript  $-1$  indicates the inverse matrix. By multiplying both sides of Eq. (10)  
 203 by the pseudo-inverse matrix  $\mathbf{X}_{1:n-1}^+$  from the right, the time evolution matrix  $\mathbf{A}$  can be  
 204 obtained as follows:

$$\mathbf{A} = \mathbf{X}_{2:n}\mathbf{V}\mathbf{\Sigma}^{-1}\mathbf{U}^*. \quad (13)$$

205 By applying the eigenvalue decomposition to the estimated  $\mathbf{A}$ , eigenvalues  $\lambda_i$  and  
 206 eigenvectors  $\psi_i(\vec{r})$  associated with the matrix  $\mathbf{A}$  are obtained for each mode ( $1 \leq i \leq$   
 207  $m$ ). Note that  $\psi_i(\vec{r})$  exhibits a discretized form in the space. Using the eigenvectors  
 208  $\psi_i(\vec{r})$ , the time-series data of  $f(\vec{r}, t)$  at position  $\vec{r}$  can be expanded as follows:

$$f(\vec{r}, t) = \sum_{i=1}^m a_i \psi_i(\vec{r}) \exp(\omega_i t), \quad (14)$$

209 where  $a_i$  and  $\omega_i$  are the amplitude (or expansion coefficient) and time constant of the  
 210  $i$ 'th mode, respectively. The time constant  $\omega_i$  can be calculated using the following  
 211 formula:

$$\omega_i = \frac{\ln(\lambda_i)}{\Delta t}. \quad (15)$$

212 Note that the prompt neutron decay constant is a negative time constant and that the  
 213 sign of  $\alpha$  is opposite to that of  $\omega_i$ , i.e.,  $\alpha_i = -\omega_i$ . In addition, the fundamental mode  
 214 component of  $\alpha$  is the slowest decay constant except for the constant background  
 215 component  $C_{BG}$  in Eq. (8) or  $P_u$  in Eq. (9) as explained in Sec. II.A. The constant  
 216 component degrades the estimation accuracy of the fundamental mode component of  $\alpha$ .  
 217 To remove the contribution of the constant background component, a constant signal for  
 218 all time steps is added virtually to matrix  $\mathbf{X}$ . By adding a constant signal, the constant  
 219 background component can be extracted as an independent mode, which contains the  
 220 first maximum eigenvalue  $\lambda_{\max} = 1$ , because the background component corresponds  
 221 to  $\exp\left(-\frac{\ln(\lambda_{\max})}{\Delta t} t\right) = 1$ . Consequently, the fundamental mode component of  $\alpha$  is  
 222 determined by the second maximum eigenvalue except for the first maximum  
 223 eigenvalue  $\lambda_{\max} = 1$  as follows:

$$\alpha = -\frac{\ln(\max(\lambda_{i'}))}{\Delta t} \text{ where } \lambda_{i'} < \lambda_{\max}. \quad (16)$$

224

### 225 **II.C. Evaluation of Statistical Uncertainty of $\alpha$ Using Randomly Sampled** 226 **Virtual Data**

227 Since the measured time-series data contain statistical errors, the random  
 228 sampling method [11] was utilized to evaluate the statistical uncertainty of  $\alpha$  in the  
 229 DMD procedure.  $N$  virtual time-series data sets were sampled by adding normal random  
 230 numbers to the elements in matrix  $\mathbf{X}$ . Here, the element of matrix  $\mathbf{X}$  in the  $i$ 'th row and  
 231  $j$ 'th column is denoted by  $x_{ij}$ . In the PNS method,  $x_{ij}$  corresponds to the neutron counts  
 232 measured by the  $i$ 'th neutron detector at the  $j$ 'th time step. By contrast, in the Rossi- $\alpha$   
 233 method,  $x_{ij}$  corresponds to the frequency of the neutron-detection-time interval  
 234 measured by the  $i$ 'th neutron detector at the  $j$ 'th time interval. If each  $x_{ij}$  has a

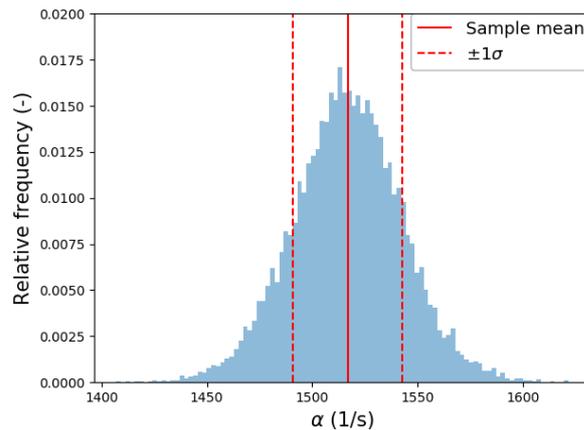
235 statistical uncertainty  $\sigma_{ij}$ , then the  $k$ 'th virtual time series data  $\mathbf{X}^{(k)}$  is generated via  
 236 perturbation as follows:

$$x_{ij}^{(k)} = x_{ij} + \sigma_{ij} \mathcal{N}(0,1), \quad (17)$$

237 where  $\mathcal{N}(0,1)$  is the standard normal random number. By applying repeatedly DMD to  
 238 each virtual data set, a histogram of  $\alpha$  can be obtained. Figure 1 shows a typical  
 239 example of a histogram for  $\alpha$ . Based on the obtained histogram of  $\alpha$ , the sample mean  
 240 and unbiased standard deviation of  $\alpha$  were estimated. The estimated standard deviation  
 241 corresponds to the statistical uncertainty of  $\alpha$  in the DMD procedure. The procedure for  
 242 calculating  $\alpha$  with statistical uncertainty is summarized as follows:

- 243 1. Create  $k$ 'th perturbed virtual time-series data by adding normal random numbers to  
 244 matrix  $\mathbf{X}^{(k)}$ .
- 245 2. Calculate time evolution matrix  $\mathbf{A}^{(k)}$  based on slicing matrices  $\mathbf{X}_{1:n-1}^{(k)}$  and  $\mathbf{X}_{2:n}^{(k)}$ .
- 246 3. Obtain eigenvalue  $\lambda_i^{(k)}$  for each mode by eigenvalue decomposition of matrix  $\mathbf{A}^{(k)}$ .
- 247 4. Evaluate the fundamental mode component of the prompt neutron decay constant  
 248  $\alpha^{(k)}$  using Eq. (16).
- 249 5. Repeat steps 1–4  $N$  times to obtain the histogram of  $\alpha$ .
- 250 6. Estimate the sample mean and standard deviation of  $\alpha$  by statistical processing for  
 251 the obtained histogram of  $\alpha$ .

252



253

254

**Figure 1. Example of histogram for  $\alpha$  by randomly sampled virtual data.**

255

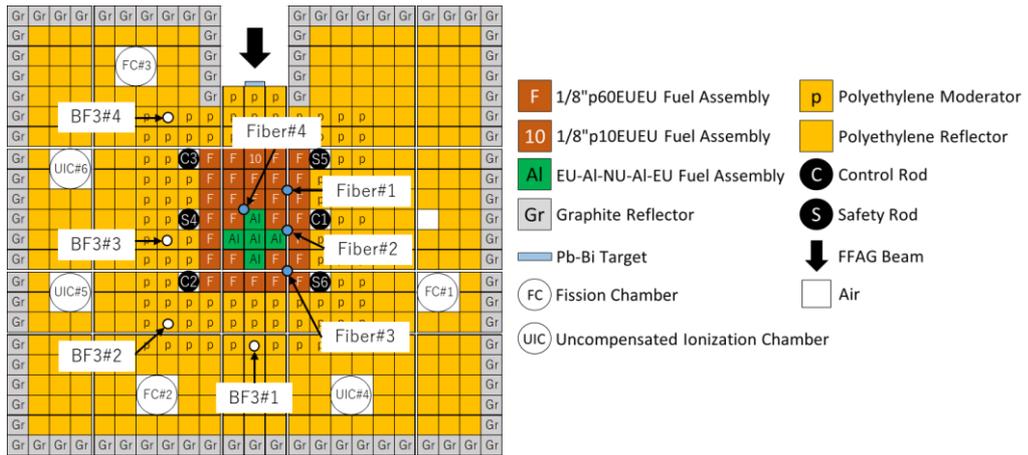
### 256 III. APPLICATION TO KUCA EXPERIMENT

#### 257 III.A. Experimental Conditions

258 The experimental KUCA core is shown in Fig. 2. All control rods (C1, C2, and  
259 C3) and safety rods (S4, S5, and S6) were fully inserted into the core in this experiment.  
260 Figure 3 shows the configurations of the fuel assemblies loaded in the core. The  
261 1/8"p60EUEU and 1/8"p10EUEU fuel assemblies were configured by a unit fuel-cell  
262 #1, which comprised two 1/16" enriched uranium plates and one 1/8" polyethylene plate.  
263 By contrast, the EU-AI-NU-AI-EU fuel assembly was configured by two different unit  
264 fuel-cells #1 and #3. Unit cell #3 comprised one natural uranium plate, four 1/16"  
265 enriched uranium plates, and four Al plates.

266 In this experiment, 100-MeV protons generated from the fixed-field alternating  
267 gradient (FFAG) accelerator were periodically injected onto the Pb-Bi target. Therefore,  
268 spallation reactions generated pulsed neutrons periodically. The beam injection period  
269 of the FFAG accelerator was 30 Hz. Using 10 neutron detectors (four BF<sub>3</sub> detectors #1–  
270 #4, four fiber-optic detectors #1–#4, two fission chambers #1–#2), the time-series data  
271 of neutron counts were measured for 1,000 s after the core reached the steady-state. In  
272 order to successfully apply DMD to the experimental data, many combinations of  
273 neutron flux with various higher mode components are necessary. Thus, as shown in Fig.  
274 2, the detectors were dispersed in asymmetrical positions to obtain the various higher  
275 mode components. In the PNS method, we analyzed the neutron count rates per one  
276 pulsed neutron-shot and the statistical uncertainties using the 30,000(=30 Hz × 1,000 s)  
277 pulsed neutron-injection results. The statistical uncertainty of the neutron count rate was  
278 evaluated by the central limit theorem. In the Rossi- $\alpha$  method, the histogram  $P(\tau)$  was  
279 obtained as the mean value of several histograms generated from the measurement  
280 results of the reactor noise for 1,000 s. Similar to the PNS experiment, the statistical  
281 uncertainty of  $P(\tau)$  was also evaluated by the central limit theorem.

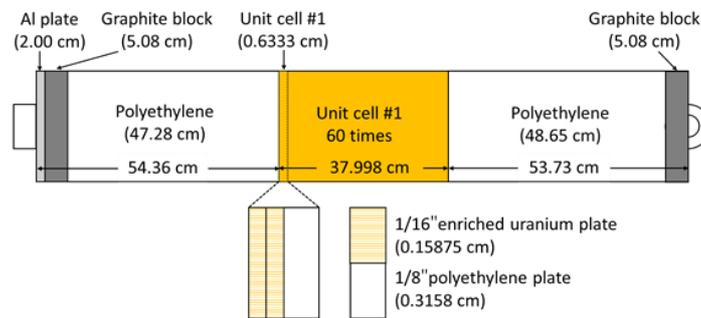
282



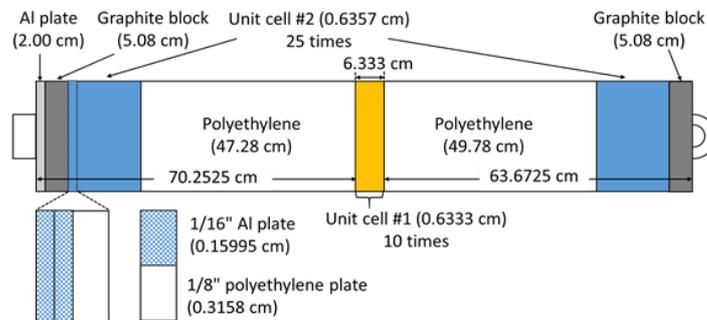
283

284

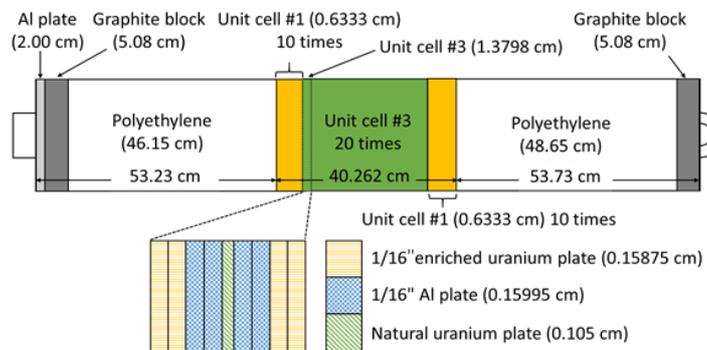
Figure 2. Top view of experimental core.



(a) 1/8''p60EUEU fuel assembly



(b) 1/8''p10EUEU fuel assembly



(c) EU-AI-NU-AI-EU fuel assembly

285

286

Figure 3. Configurations of fuel assemblies.

287 Table 1 shows the control rod worth measured by the rod drop method [12] and  
 288 the excess reactivity of the experimental core measured by the positive period method  
 289 [12]. To evaluate the rod worth and excess reactivity, the decay constants  $\lambda_i$  and the  
 290 relative yields  $a_i$  for delayed neutrons were taken from the Keepin data [13]. As shown  
 291 in Fig. 2, the control rods and safety rods were arranged symmetrically. Therefore, it  
 292 was assumed that the rod worth of the safety rod was equal to that of the control rod at  
 293 the symmetric position. Table 1 also shows the subcriticality ( $-\rho$ ) of the experimental  
 294 core calculated from the rod worth and the excess reactivity. The uncertainty of each  
 295 value presented in Table 1 was evaluated using the random sampling method [11] to  
 296 consider the normal-distributed uncertainties of  $\lambda_i$ ,  $a_i$  [13] and the measured doubling  
 297 time, as well as Poisson-distributed statistical errors of neutron counts in the rod drop  
 298 method. In the random sampling method, the sum of the perturbed  $a_i$  was normalized to  
 299 unity, and the sample size was set to 10,000 to estimate the uncertainties of the rod  
 300 worth, excess reactivity, and ( $-\rho$ ).

301  
302

**Table 1. Experimental results of rod drop method and period method.**

Rod worth (\$)	C1, S4	$1.203 \pm 0.041$
	C2, S6	$0.408 \pm 0.014$
	C3, S5	$0.408 \pm 0.014$
Excess reactivity (\$)		$0.036 \pm 0.001$
Subcriticality ( $-\rho$ ) (\$)		$4.001 \pm 0.133$

303  
304  
305  
306  
307  
308  
309  
310  
311  
312

Table 2 shows the effective delayed neutron fraction  $\beta_{\text{eff}}$  and the neutron generation time  $\Lambda$  for the experimental core calculated by MCNP6.2 [14] with ENDF/B-VII.1 [15]. In Table 2, the uncertainties in  $\beta_{\text{eff}}$  and  $\Lambda$  are the statistical errors due to MCNP6.2. Based on the fundamental mode approximation, the prompt neutron decay constant  $\alpha$  assumed to be nearly equal to  $(\beta_{\text{eff}} - \rho)/\Lambda$ . For comparison with the measured  $\alpha$ , Table 2 also presents the value of  $(\beta_{\text{eff}} - \rho)/\Lambda$  using the experimental result of ( $-\rho$ ) and the numerical results of  $\Lambda$  and  $\beta_{\text{eff}}$ . Similar to Table 1, the uncertainty of  $(\beta_{\text{eff}} - \rho)/\Lambda$  was evaluated using the random sampling method.

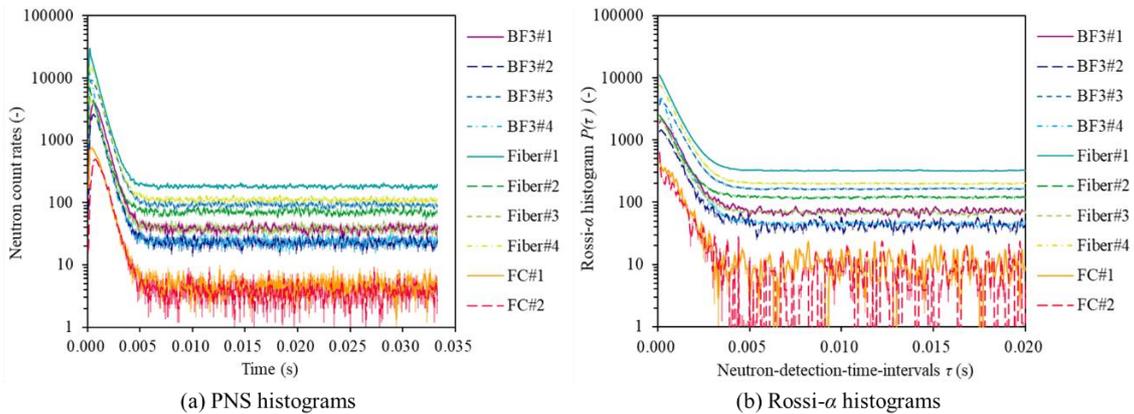
313 **Table 2. Calculation results of point kinetics parameters and  $(\beta_{\text{eff}} - \rho)/\Lambda$ .**

Effective delayed neutron fraction $\beta_{\text{eff}}$ (-)	$0.00797 \pm 0.00006$
Neutron generation time $\Lambda$ ( $\mu\text{s}$ )	$27.20 \pm 0.04$
$(\beta_{\text{eff}} - \rho)/\Lambda$ (1/s)	$1466 \pm 39$

### 314 III.B. Experimental Results and DMD Analysis

315 The time-series data of the PNS and Rossi- $\alpha$  methods were successively  
 316 measured using 10 neutron detectors (four BF<sub>3</sub> detectors, four fiber-optic detectors, and  
 317 two fission chambers). The positions of the detectors in the experimental core are  
 318 shown in Fig. 2. In the PNS method, neutrons were successively counted by a time step  
 319 of  $\Delta t = 0.0001$  (s). In the Rossi- $\alpha$  method, the frequency of neutron-detection-time  
 320 interval was also calculated by a time bin of  $\Delta \tau = 0.0001$  (s). Figure 4 shows the  
 321 experimental results obtained by the PNS and Rossi- $\alpha$  methods. In the DMD, matrices  $\mathbf{X}$   
 322 was constructed using both time-series data shown in Fig. 4, respectively. From Fig. 4-  
 323 (a), the size of the matrix  $\mathbf{X}$  in the PNS method was  $10 \times 333$ , i.e., 333 time steps were  
 324 measured with 10 neutron detectors. Meanwhile, from Fig. 4-(b), the size of matrix  $\mathbf{X}$  in  
 325 the Rossi- $\alpha$  method was  $10 \times 200$ , i.e., 200 time intervals were measured with 10  
 326 neutron detectors. In addition, constant signals of 1 for all time steps were virtually  
 327 added to both matrices  $\mathbf{X}$ , in order to remove the constant components shown in Eqs. (8)  
 328 and (9) in the DMD procedure.

329



330

331 **Figure 4. Experimental results of the PNS and Rossi- $\alpha$  method.**

332

333 Figure 5 shows the results of applying DMD and the conventional fitting method  
 334 to the PNS method. Similarly, Fig. 6 shows the results of applying the aforementioned  
 335 methods to the Rossi- $\alpha$  method. The horizontal axes in Figs. 5 and 6 represent the  
 336 masking time for excluding the effect of higher mode components. For comparison, the  
 337 calculated  $(\beta_{\text{eff}} - \rho)/\Lambda$  value shown in Table 2 is also presented in Figs. 5 and 6. In the

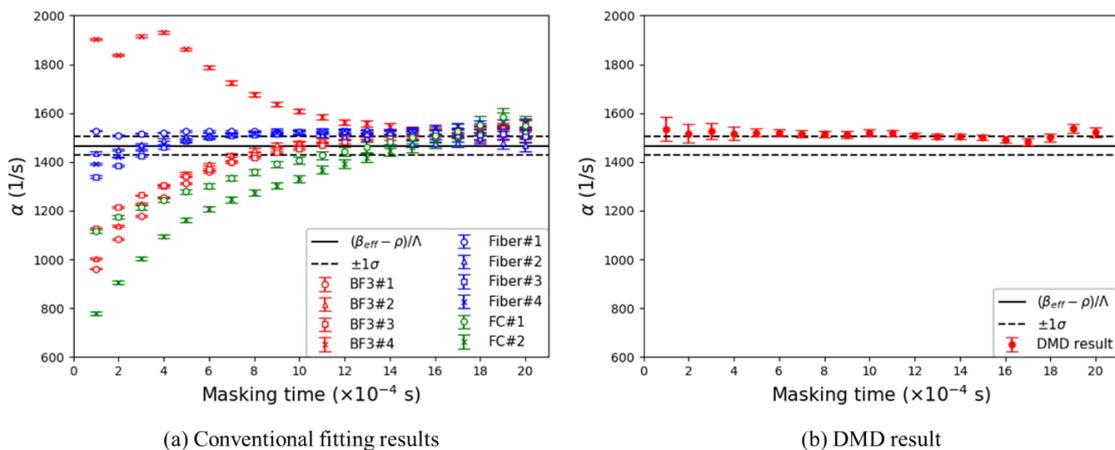
338 conventional fitting method, the PNS and Rossi- $\alpha$  histograms shown in Fig. 4 were  
 339 fitted by the following formulas, respectively:

$$C(t) = C_0 \exp(-\alpha t) + C_{BG}, \quad (18)$$

$$P(\tau) = P_0 \exp(-\alpha \tau) + P_u, \quad (19)$$

340 where  $C_0$ ,  $C_{BG}$ ,  $P_0$ , and  $P_u$  are fitting parameters, and  $\alpha$  is the prompt neutron decay  
 341 constant. To obtain the least-squares fitting results shown in Figs 5-(a) and 6-(a), the  
 342 “scipy.optimize.curve\_fit” module [16] was utilized. By setting the option of  
 343 “absolute\_sigma” to “True,” the fitting error of  $\alpha$  was evaluated using the absolute value  
 344 of the statistical uncertainty ( $1\sigma$ ) at each time step. Note that the fitting error in this  
 345 study was approximately estimated without considering the covariance between the  
 346 different time steps. Hence, the fitting errors of  $\alpha$  shown in Fig. 5-(a) and Fig. 6-(a)  
 347 were underestimated, compared with the bias between the fitting result and  
 348  $(\beta_{\text{eff}} - \rho)/\Lambda$ . By contrast, in the DMD, the fundamental mode component of  $\alpha$  and the  
 349 statistical uncertainty were estimated as described in Sec. II.C. The sample size  $N$  for  
 350 evaluating the statistical uncertainty of  $\alpha$  was set as  $N = 10,000$  such that the relative  
 351 statistical error of the uncertainty estimated by the random sampling method was less  
 352 than 1%. When  $N = 10,000$ , the relative statistical error of the uncertainty using the  
 353 random sampling method is expected to be  $1/\sqrt{2(N-1)} \approx 0.7\%$  [17].

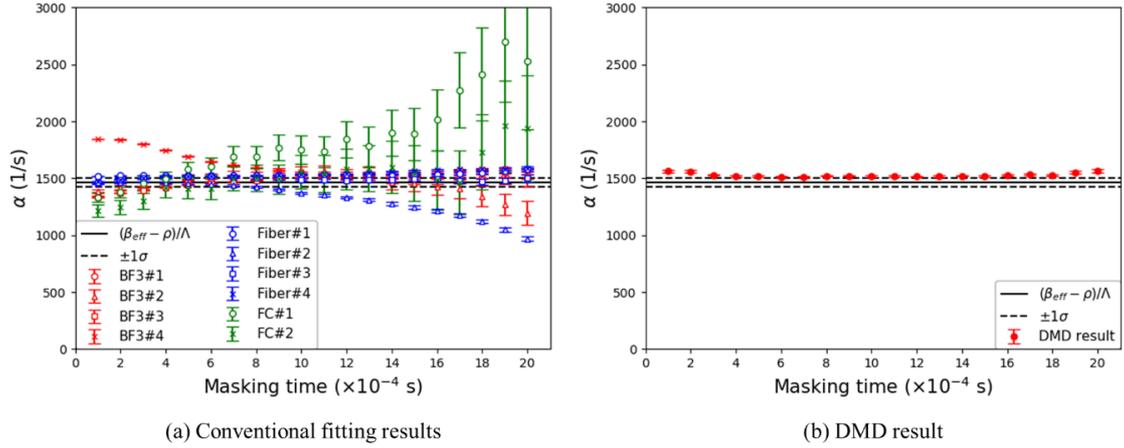
354



355

356

**Figure 5. Estimation results of  $\alpha$  by PNS method.**



(a) Conventional fitting results

(b) DMD result

**Figure 6. Estimation results of  $\alpha$  by Rossi- $\alpha$  method.**

357

358

### 359 III.C. Discussion

360 In the early stage of the time steps of the PNS and Rossi- $\alpha$  histograms, the  
 361 higher mode components do not necessarily decay sufficiently. Using the conventional  
 362 fitting method, the effect of the higher mode component becomes significant in the  
 363 early stage of decay. For example, in the case of the PNS method as shown in Fig. 5-(a),  
 364 the conventional fitting results of the BF<sub>3</sub> detectors and fission chambers deviated  
 365 significantly from the  $(\beta_{\text{eff}} - \rho)/\Lambda$  value as the masking time decreased. Also in the  
 366 case of the Rossi- $\alpha$  method as shown in Fig. 6-(a), a similar trend was also observed for  
 367 the BF<sub>3</sub> detectors and fission chambers. These differences between the conventional  
 368 fitting results and the  $(\beta_{\text{eff}} - \rho)/\Lambda$  value were greater than the fitting error of  $\alpha$ , i.e., the  
 369 conventional fitting results contained large systematic errors due to the higher mode  
 370 components in the early stages of decay.

371 Meanwhile, for the Rossi- $\alpha$  method, as the masking time increased, the fitting  
 372 results of  $\alpha$  for BF<sub>3</sub>#2, Fiber#2, and fission chambers deviated from the  $(\beta_{\text{eff}} - \rho)/\Lambda$   
 373 value, as shown in Fig. 6-(a). This is because the decay of the fundamental mode  
 374 component could not be easily extracted when the masking time to eliminate the effect  
 375 of higher mode components was too large, i.e, the histograms after masking were  
 376 almost constant. Furthermore, the larger variations in the fitting results of  $\alpha$  for FC#1  
 377 and FC#2 with respect to the masking time were observed due to the larger statistical  
 378 uncertainties of the Rossi- $\alpha$  histograms for FC#1 and FC#2, as shown in Fig. 4-(b).

379 As discussed above, the appropriate masking time must be carefully selected to  
 380 appropriately estimate the fundamental mode component of  $\alpha$  using the conventional  
 381 fitting method. However, the determination of masking time is difficult because the

382 reference value of  $\alpha$  is usually unknown beforehand. In addition, since multiple  
383 detectors were used in this experiment, the conventional fitting method yielded different  
384 estimation results of  $\alpha$  for each detector, i.e., the selection of an appropriate detector to  
385 obtain the fundamental mode component of  $\alpha$  was not straightforward. To summarize,  
386 in the conventional fitting method, it is difficult to uniquely determine the value of  $\alpha$   
387 only from the measurement results.

388 By contrast, in DMD, the influence of higher mode components could be  
389 eliminated from the fundamental mode component by decomposing the time-series data  
390 into multiple exponential modes. Therefore, even in the early stages of decay, the  
391 fundamental mode component of  $\alpha$  can be extracted robustly. Consequently, the  
392 variation in the estimated  $\alpha$  with respect to the masking time could be reduced  
393 significantly, as shown in Figs. 5-(b) and 6-(b). DMD enables us to robustly estimate  
394 the fundamental mode component of  $\alpha$  even when the reference value is unknown. The  
395 masking time in DMD can be determined simply to minimize the statistical uncertainty  
396 of  $\alpha$ . For example, the DMD results of  $\alpha$  with the smallest statistical uncertainty were  
397  $1505 \pm 10$  (1/s) and  $1519 \pm 4$  (1/s) for the PNS and Rossi- $\alpha$  experiments, respectively.  
398 Furthermore, even when multiple detectors were used, DMD provided a unique result  
399 for  $\alpha$  from all the detector data. Hence, it was confirmed that DMD addressed the issue  
400 of the conventional fitting method because it is easy to uniquely determine the  
401 fundamental mode component of  $\alpha$ .

402

#### 403 **IV. CONCLUSIONS**

404 Using DMD and randomly sampled virtual data, the present paper attempted to  
405 investigate the prompt neutron decay constant  $\alpha$  of the fundamental mode component  
406 with statistical uncertainty. To demonstrate our proposed technique, experimental  
407 analyses by the PNS and Rossi- $\alpha$  methods were performed. In applying the DMD to the  
408 PNS and Rossi- $\alpha$  experimental data, the background constant component was removed  
409 by adding a constant signal to the experimental data. Consequently, the estimation  
410 results for the fundamental mode component of  $\alpha$  were approximately constant with  
411 respect to the masking time, as compared with the larger variation in the conventional  
412 fitting  $\alpha$  value. In conclusion, DMD enabled one to robustly estimate the fundamental  
413 mode component of  $\alpha$  in the PNS and Rossi- $\alpha$  methods, and the applicability of DMD to  
414 both methods was demonstrated.

415

## 416 ACKNOWLEDGMENTS

417 This study has been carried out under the visiting researcher's program at the  
418 Kyoto University Institute for Integrated Radiation and Nuclear Science. This study was  
419 supported by the Japan Society for the Promotion of Science (JSPS) Grant-in-Aid for  
420 Scientific Research (C). [Grant Number 19K05328].

421

## 422 REFERENCES

- 423 1. T. ENDO and A. YAMAMOTO, "Data Assimilation Using Subcritical Measurement  
424 of Prompt Neutron Decay Constant," *Nucl. Sci. Eng.*, **194**, 11, 1089 (2020);  
425 <https://doi.org/10.1080/00295639.2020.1720499>.
- 426 2. B. E. SIMMONS and J. S. KING, "A Pulsed Neutron Technique for Reactivity  
427 Determination," *Nucl. Sci. Eng.*, **3**, 5, 595 (1958);  
428 <https://doi.org/10.13182/NSE3-595-608>.
- 429 3. J. D. ORNDOFF, "Prompt Neutron Periods of Metal Critical Assemblies," *Nucl. Sci.*  
430 *Eng.*, **2**, 4, 450 (1957); <https://doi.org/10.13182/NSE57-A25409>.
- 431 4. R. KATANO, "Estimation Method of Prompt Neutron Decay Constant Reducing  
432 Higher Order Mode Effect by Linear Combination," *Nucl. Sci. Eng.*, **193**, 4, 431  
433 (2019); <https://doi.org/10.1080/00295639.2018.1528803>.
- 434 5. R. KATANO, M. YAMANAKA, and C. H. PYEON, "Application of Linear  
435 Combination Method to Pulsed Neutron Source Measurement at Kyoto University  
436 Critical Assembly," *Nucl. Sci. Eng.*, **193**, 12, 1394 (2019);  
437 <https://doi.org/10.1080/00295639.2019.1624084>.
- 438 6. R. KATANO, M. YAMANAKA, and C.H. PYEON, "Measurement of prompt  
439 neutron decay constant with spallation neutrons at Kyoto University Critical  
440 Assembly using linear combination method," *J. Nucl. Sci. Technol.*, **57**, 2, 169  
441 (2020); <https://doi.org/10.1080/00223131.2019.1671911>.
- 442 7. P. J. SCHMID, "Dynamic mode decomposition of numerical and experimental  
443 data," *J. Fluid Mech.*, **656**, 5 (2010); <https://doi.org/10.1017/S0022112010001217>.

- 444 8. Z. K. HARDY, J. E. MOREL, and C. AHRENS, “Dynamic Mode Decomposition  
445 for Subcritical Metal Systems,” *Nucl. Sci. Eng.*, **193**, 11, 1173 (2019);  
446 <https://doi.org/10.1080/00295639.2019.1609317>.
- 447 9. T. ENDO, Y. YAMANE, and A. YAMAMOTO, “Space and energy dependent  
448 theoretical formula for the third order neutron correlation technique,” *Ann. Nucl.*  
449 *Energy.*, **33**, 6, 521 (2006); <https://doi.org/10.1016/j.anucene.2006.02.002>.
- 450 10. P. BAETEN, “Heuristic derivation of the Rossi-alpha formula for a pulsed neutron  
451 source,” *Ann. Nucl. Energy.*, **31**, 1, 43 (2004);  
452 [https://doi.org/10.1016/S0306-4549\(03\)00162-2](https://doi.org/10.1016/S0306-4549(03)00162-2).
- 453 11. T. ENDO et al., “Subcriticality measurement using time-domain decomposition-  
454 based integral method for simultaneous reactivity and source changes,” *J. Nucl. Sci.*  
455 *Technol.*, **57**, 5, 607 (2020); <https://doi.org/10.1080/00223131.2019.1706658>.
- 456 12. T. MISAWA, H. UNESAKI, and C. H. PYEON, *Nuclear Reactor Physics*  
457 *Experiments*, Kyoto University Press, Kyoto, Japan (2010).
- 458 13. G. R. KEEPIN, *Physics of Nuclear Kinetics*, Addison-Wesley Pub. Co., Inc.,  
459 Reading, MA (1965).
- 460 14. “MCNP User’s Manual Code Version 6.2,” LA-UR-17-29981, C. J. WERNER, Ed.,  
461 Los Alamos National Laboratory (Oct. 2017).
- 462 15. M. B. CHADWICK et al., “ENDF/B-VII.1 Nuclear Data for Science and  
463 Technology: Cross Sections, Covariances, Fission Product Yields and Decay Data,”  
464 *Nucl. Data Sheets*, **112**, 12, 2887 (2011); <https://doi.org/10.1016/j.nds.2011.11.002>.
- 465 16. “scipy.optimize.curve\_fit — SciPy v1.6.2 Reference Guide,”  
466 [https://docs.scipy.org/doc/scipy/reference/generated/scipy.optimize.curve\\_fit.html](https://docs.scipy.org/doc/scipy/reference/generated/scipy.optimize.curve_fit.html);  
467 (current as of Apr. 16, 2021).
- 468 17. B. FOAD, A. YAMAMOTO, and T. ENDO, “Uncertainty and regression analysis of  
469 the MSLB accident in PWR based on unscented transformation and low rank  
470 approximation,” *Ann. Nucl. Energy.*, **143**, 107493 (2020);  
471 <https://doi.org/10.1016/j.anucene.2020.107493>.
- 472

473 **List of Tables**

474 Table 1. Experimental results of rod drop method and period method.

475 Table 2. Calculation results of point kinetics parameters and  $(\beta_{\text{eff}} - \rho)/\Lambda$ .

476

477 **List of Figures**

478 Figure 1. Example of histogram for  $\alpha$  by randomly sampled virtual data.

479 Figure 2. Top view of experimental core.

480 Figure 3. Configurations of fuel assemblies.

481 Figure 4. Experimental results of the PNS and Rossi- $\alpha$  method.

482 Figure 5. Estimation results of  $\alpha$  by PNS method.

483 Figure 6. Estimation results of  $\alpha$  by Rossi- $\alpha$  method.