

# Momentum removal to obtain the position-dependent diffusion constant in constrained molecular dynamics simulation

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The position-dependent diffusion coefficient along with free energy profile are important parameters needed to study mass transport in heterogeneous systems such as biological and polymer membranes, and molecular dynamics (MD) calculation is a popular tool to obtain them. Among many methodologies, the Marrink–Berendsen (MB) method is often employed to calculate the position-dependent diffusion coefficient, in which the autocorrelation function of the force on a fixed molecule is related to the friction on the molecule. However, the diffusion coefficient is shown to be affected by the period of the removal of the center-of-mass velocity,  $\tau_{v0}$ , which is necessary when performing MD calculations using the Ewald method for Coulombic interaction. We have clarified theoretically in this study how this operation affects the diffusion coefficient calculated by the MB method, and the theoretical predictions are proven by MD calculations. Therefore, we succeeded in providing guidance on how to select an appropriate  $\tau_{v0}$  value in estimating the position-dependent diffusion coefficient by the MB method. This guide-

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**Abbreviations:** COM, Center of mass; FACF, Force autocorrelation function; MB, Marrink–Berendsen; MD, Molecular Dynamics; WR, Woolf–Roux.

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line is applicable also to the Woolf–Roux method.

## KEYWORDS

Position-dependent diffusion coefficient, Marrink–Berendsen method, Woolf–Roux method, Molecular dynamics calculation

## 24 | 1 | INTRODUCTION

25 Mass transport phenomena in heterogeneous systems are important issues in various fields, and much research has  
26 been conducted in this area to date. For example, in the field of biological chemistry, understanding the permeation  
27 of drugs into viruses<sup>1</sup> and through membranes<sup>2–4</sup> at the molecular level plays an important role in appropriate ra-  
28 tional drug design. In the field of materials sciences such as in the separation of molecules using reverse osmosis  
29 membranes<sup>5,6</sup> and the study of the transport process of protons, oxygen, and hydrogen in a polymer electrolyte  
30 membrane<sup>7–9</sup>, it is important to understand the relationship between the mechanism of molecular transport and the  
31 microscopic details of the materials.

32 The position-dependent diffusion coefficient, along with the free energy profile, is an important physical quantity  
33 utilized in studies of the mass transport phenomena of heterogeneous systems using molecular dynamics (MD) calcu-  
34 lations. Because of its importance, many methods<sup>10–19</sup> have been proposed to obtain the position-dependent diffu-  
35 sion coefficient. Two of us and other coworkers have also previously proposed a method for obtaining the position-  
36 dependent diffusion coefficient with high accuracy in any heterogeneous system<sup>20</sup>.

37 Among the methods proposed so far, the Marrink–Berendsen (MB) method is one of the best-known methods  
38 used to calculate the position-dependent diffusion coefficient<sup>21–26</sup>. This method allows for straightforward calcu-  
39 lation of the the position-dependent diffusion coefficient with existing MD calculation packages. In this method,  
40 the center of mass (COM) of the molecule is constrained to a certain position, and the diffusion coefficient can be  
41 obtained by the force autocorrelation function (FACF) of the COM of the molecule. A downside is systematic un-  
42 derestimation of the resultant diffusion coefficient<sup>27,20</sup>, which can be attributed to perturbation of dynamics arising  
43 from constraints. In other words, the memory kernel of a freely moving particle may not always be well approximated  
44 by that of a constrained particle.

45 In this paper, we demonstrate the critical role of momentum removal in obtaining the position-dependent dif-  
46 fusion coefficient by methods involving position constraints, such as the MB method. In MD calculations that use  
47 the Ewald method<sup>28,29</sup> for calculating the long-range Coulombic interaction, the momentum of the MD system is  
48 reduced to zero with a certain time interval,  $\tau_{V0}$ , to prevent the MD system from diffusing. We demonstrate that this  
49 operation affects the diffusion coefficient calculated by the MB method when constraining the diffusing molecules  
50 to absolute coordinates. In particular, the diffusion coefficient can be overestimated without the operation. In this  
51 paper, we propose a theoretical equation comparing FACFs with and without the COM momentum removal. The  
52 theoretical equation was then examined to find the diffusion coefficient of methane in water. It was also found that  
53  $\tau_{V0}$  dependence varies with the size of the system in the MD calculation. The theory we propose in this paper plays  
54 an important role in obtaining the position-dependent diffusion coefficient in three-dimensional heterogeneous sys-  
55 tems using the MB method. The method with spring restraint on absolute values, proposed by Woolf and Roux (WR  
56 method),<sup>12</sup> is also discussed.

57 **2 | THEORY**

58 The change in FACF,  $\langle \mathbf{F}(0) \cdot \mathbf{F}(t) \rangle$ , with changing  $\tau_{v0}$  is explained qualitatively in terms of the momentum conservation  
 59 within the whole simulation cell. Suppose that a solute molecule of infinite dilution feels force from the surrounding  
 60 solvent in the  $+z$  direction at  $t = 0$ . The force between the solute and the solvent means the momentum exchange  
 61 between them, and the momentum in the  $-z$  direction is then transferred from the solute to the solvent. The momen-  
 62 tum given by the solvent is further transported to the bulk solvent with time through solvent-solvent interactions. In  
 63 the MD simulation cell of finite size, however, the momentum in the  $-z$  direction cannot dissipate due to the momen-  
 64 tum conservation, and the momentum is instead distributed uniformly over the whole simulation cell after sufficient  
 65 time, which means the solvent flows in the  $-z$  direction. The fixed solute in the solvent flow in the  $-z$  direction then  
 66 feels frictional force in the  $-z$  direction, leading to a negative correlation between  $\mathbf{F}(0)$  and  $\mathbf{F}(t)$ . A shift of the COM  
 67 velocity of the solvent eliminates the negative correlation, and its operation frequency,  $1/\tau_{v0}$ , affects the strength of  
 68 the negative correlation at longer time durations. The physics concepts outlined above are described quantitatively  
 69 hereafter in this section using projection operator formalism.

70 The system under consideration is composed of a solute (X) and a finite number of solvent molecules (S), which  
 71 are contained in a cell with periodic boundary conditions. The solute is fixed at a given spatial position and no other  
 72 external force operates on the solvent. A shift of the COM velocity of the solvent is not performed.

73 The COM velocity of the solvent,  $\mathbf{v}_{CM}$ , is defined as follows:

$$\mathbf{v}_{CM} \equiv \frac{1}{M_S} \sum_{i \in S} m_i \mathbf{v}_i, \quad (1)$$

$$M_S \equiv \sum_{i \in S} m_i. \quad (2)$$

74 Here, the summations run over all the solvent molecules, and the mass and the velocity of the  $i$ -th solvent molecule  
 75 are described as  $m_i$  and  $\mathbf{v}_i$ , respectively. The projection operator onto  $\mathbf{v}_{CM}$  is defined as  $\mathcal{P}$ , and the projection operator  
 76 to the orthogonal space is given by  $Q \equiv 1 - \mathcal{P}$ . The definition of the projection operator,  $\mathcal{P}$ , is explicitly given by

$$\mathcal{P}\mathbf{A} \equiv \frac{\langle \mathbf{v}_{CM} \cdot \mathbf{A} \rangle}{\langle |\mathbf{v}_{CM}|^2 \rangle} \mathbf{v}_{CM} = \frac{M_S}{3k_B T} \langle \mathbf{v}_{CM} \cdot \mathbf{A} \rangle \mathbf{v}_{CM}, \quad (3)$$

77 where  $\mathbf{A}$  is an arbitrary vector variable. The Boltzmann constant and the absolute temperature are denoted here as  
 78  $k_B$  and  $T$ , respectively.

79 An identity below holds for the time propagation operator as<sup>30</sup>

$$e^{j\mathcal{L}t} Q = e^{iQ\mathcal{L}Qt} + \int_0^t d\tau e^{j\mathcal{L}(t-\tau)} \mathcal{P} i \mathcal{L} e^{iQ\mathcal{L}Q\tau}, \quad (4)$$

80 where  $\mathcal{L}$  stands for the Liouvillian operator. Equation (4) is then multiplied by the force on the solute,  $\mathbf{F}_X$ , from the  
 81 left to yield

$$\begin{aligned} e^{j\mathcal{L}t} \mathbf{F}_X &= e^{iQ\mathcal{L}Qt} \mathbf{F}_X - \frac{M_S}{3k_B T} \int_0^t d\tau \left[ e^{j\mathcal{L}(t-\tau)} \mathbf{v}_{CM} \right] \\ &\quad \times \left\langle \left\{ i \mathcal{L} \mathbf{v}_{CM} \right\} \cdot \left\{ e^{iQ\mathcal{L}Q\tau} \mathbf{F}_X \right\} \right\rangle. \end{aligned} \quad (5)$$

82 The Hermitian property of the Liouvillian operator,

$$\langle \mathbf{A} \cdot \{i\mathcal{L}\mathbf{B}\} \rangle = - \langle \{i\mathcal{L}\mathbf{A}\} \cdot \mathbf{B} \rangle, \quad (6)$$

83 is utilized in the derivation from Equations (4) to (5), where  $\mathbf{A}$  and  $\mathbf{B}$  stand for arbitrary vector quantities.

84 The momentum conservation of the whole system relates  $\mathbf{F}_X$  and  $\mathbf{v}_{CM}$  as

$$\mathbf{F}_X + M_S \{i\mathcal{L}\mathbf{v}_{CM}\} = 0, \quad (7)$$

85 which is substituted into Eq. (5) to give

$$\begin{aligned} e^{i\mathcal{L}t}\mathbf{F}_X &= e^{iQ\mathcal{L}Qt}\mathbf{F}_X + \frac{1}{3k_B T} \int_0^t d\tau \left[ e^{i\mathcal{L}(t-\tau)}\mathbf{v}_{CM} \right] \\ &\times \left\langle \mathbf{F}_X \cdot \left\{ e^{iQ\mathcal{L}Q\tau}\mathbf{F}_X \right\} \right\rangle. \end{aligned} \quad (8)$$

86 We change the notations here as follows:

$$\mathbf{F}_X(t) \equiv e^{i\mathcal{L}t}\mathbf{F}_X, \quad (9)$$

$$\mathbf{R}_X(t) \equiv e^{iQ\mathcal{L}Qt}\mathbf{F}_X, \quad (10)$$

$$\mathbf{v}_{CM}(t) \equiv e^{i\mathcal{L}t}\mathbf{v}_{CM}, \quad (11)$$

$$\gamma(t) \equiv \frac{1}{3k_B T} \langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle. \quad (12)$$

87 Equation (8) is then rewritten with these notations as

$$\mathbf{F}_X(t) = \mathbf{R}_X(t) + \int_0^t d\tau \gamma(t-\tau)\mathbf{v}_{CM}(\tau). \quad (13)$$

88 In Eq. (13), the total force acting on the solute at time  $t$ ,  $\mathbf{F}_X(t)$ , is divided into the sum of random force,  $\mathbf{R}_X(t)$ , and  
89 the drag force by the flow of the solvent.

90 The statistical average of Eq. (13) after the multiplication of  $\mathbf{F}_X(0) = \mathbf{R}_X(0)$  gives

$$\begin{aligned} \langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle &= \langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle + \int_0^t d\tau \gamma(t-\tau) \\ &\times \langle \mathbf{F}_X(0) \cdot \mathbf{v}_{CM}(\tau) \rangle. \end{aligned} \quad (14)$$

91 The time correlation function in the integral,  $\langle \mathbf{F}_X(0) \cdot \mathbf{v}_{CM}(\tau) \rangle$ , is further related to FACF as

$$\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle + M_S \frac{d}{dt} \langle \mathbf{F}_X(0) \cdot \mathbf{v}_{CM}(t) \rangle = 0 \quad (15)$$

92 by virtue of Eq. (7).

93 The MB method is used to evaluate approximately the time correlation function of the random force acting on a  
94 freely moving solute as that of the total force on the spatially fixed one<sup>11</sup>. The time correlation function of the random  
95 force is then converted into the time-dependent friction coefficient through Eq. (12), and the position-dependent  
96 diffusion coefficient can then be determined. According to Eq. (14), however, the time correlation function of the

97 total force,  $\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle$ , contains the correlation with the drag force, in addition to the time correlation function  
 98 of the random force,  $\langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle$ . What we actually want to determine is the latter correlation function, and we  
 99 need to somehow eliminate the second term of Eq. (14).

100 The time development of the random force is governed by the projected Liouvillian,  $QLQ$ , instead of the normal  
 101 one,  $\mathcal{L}$ . Since the dynamics of the random force are determined by that of the positions and the momenta of the  
 102 solvent molecules,  $\{\mathbf{r}_i, \mathbf{p}_i\}$ , the effects of the replacement of the Liouvillian can be analyzed through their dynamics.  
 103 The time dependence of  $\mathbf{r}_i$  and  $\mathbf{p}_i$  through  $QLQ$  is explicitly written as follows:

$$iQLQ\mathbf{r}_i = \frac{1}{m_i}\mathbf{p}_i - \frac{1}{M_S}\sum_{j \in S}\mathbf{p}_j, \quad (16)$$

$$iQLQ\mathbf{p}_i = \mathbf{F}_i - \frac{m_i}{M_S}\sum_{j \in S}\mathbf{F}_j, \quad (17)$$

104 where  $\mathbf{F}_i$  stands for the force acting on the solvent molecule  $i$ . The derivation of these equations is described in  
 105 Sec. S1 of Supporting Information. In Eqs. (16) and (17), the first terms of the right-hand sides give the ordinary  
 106 time dependence through  $\mathcal{L}$ , and the second terms mean the shift of the COM velocity. Therefore, the dynamics  
 107 given by the projected Liouvillian,  $QLQ$ , corresponds to the time propagation of MD simulation in which the shift  
 108 of the COM velocity is performed at every step, and the autocorrelation function of the force in such MD simulation  
 109 can be regarded as that of  $\mathbf{R}_X(t)$ . It is thus expected that a smaller  $\tau_{v0}$  leads to a better diffusion coefficient in the  
 110 implementation of the MB method in MD simulation.

111 The long-time limiting behaviors of  $\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle$  can be analyzed based on Eqs. (14) and (15). First, the integral  
 112 of Eq. (15) from  $t = 0$  to  $\infty$  gives

$$\int_0^\infty dt \langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle = M_S [\langle \mathbf{F}_X(0) \cdot \mathbf{v}_{CM(0)} \rangle - \langle \mathbf{F}_X(0) \cdot \mathbf{v}_{CM(\infty)} \rangle]. \quad (18)$$

113 The first term of the right-hand side vanishes so long as  $\mathbf{F}_X$  does not depend on the velocity of the solvent explicitly.  
 114 The second term is also zero because the correlation is lost after the infinite time interval. Therefore, the integral of  
 115  $\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle$  on the left-hand side is equal to zero. It should be noted that the discussion above does not apply to  
 116 an infinite-size system where  $M_S$  diverges.

117 The time derivative of Eq. (14), combined with Eq. (15) yields

$$\begin{aligned} \frac{d}{dt} \langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle &= \frac{d}{dt} \langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle \\ &\quad - \frac{1}{M_S} \int_0^t d\tau \gamma(t-\tau) \langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(\tau) \rangle. \end{aligned} \quad (19)$$

118 Provided that the relaxation of  $\gamma(t)$  is relatively fast, Eq. (19) can be approximated in the time scale longer than the  
 119 relaxation time of  $\gamma(t)$  as

$$\begin{aligned} &\frac{d}{dt} \langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle \\ &\simeq -\frac{1}{M_S} \left[ \int_0^\infty d\tau \gamma(\tau) \right] \langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle. \end{aligned} \quad (20)$$

120 It means that  $\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle$  decays exponentially as

$$\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle \propto e^{-\frac{t}{\tau_{FF}}}, \quad (21)$$

121 with the time constant given by

$$\tau_{FF} = \frac{M_S}{\int_0^\infty d\tau \gamma(\tau)}. \quad (22)$$

## 122 3 | METHOD

### 123 3.1 | Molecular dynamics calculation

124 The effect of the frequency of the shift of the COM velocity on the time correlation function was investigated by  
 125 performing simulations with different  $\tau_{v0}$  values. Here,  $\tau_{v0}$  denotes the interval between the removals of the COM  
 126 velocity during MD simulations. System-size dependence was also investigated by studying two methane solutions  
 127 of different sizes. The smaller system was composed of a methane molecule and 1053 water molecules and was  
 128 simulated with  $\tau_{v0}$  set at 1 fs, 0.1 ps, 10 ps, and  $\infty$ . As to the larger system consisting of a methane molecule and  
 129 8424 water molecules,  $\tau_{v0}$  was set at 0.1 ps, 10 ps, and  $\infty$ . Since the time step of the MD simulation was set at 1 fs as  
 130 described below, the simulation with  $\tau_{v0} = 1$  fs corresponds to a faithful realization of the dynamics as defined by Eqs.  
 131 16 and 17, whereby  $\mathbf{R}_X(t)$  can be directly and accurately evaluated. Moreover, simulations with  $\tau_{v0} = \infty$  correspond  
 132 to the dynamics defined by the Liouvillian operator. These simulations enable the measurement of  $\mathbf{F}_X(t)$ . Hereafter,  
 133 the FACF obtained by MD with  $\tau_{v0}$  is denoted by  $C_{FF}^{\text{sim}}(t; \tau_{v0}) \equiv \langle \mathbf{F}^{\text{sim}}(t; \tau_{v0}) \cdot \mathbf{F}^{\text{sim}}(0; \tau_{v0}) \rangle$  to explicitly express the  
 134 dependence on  $\tau_{v0}$ .

135 After routine equilibration, each of the production runs was performed in the NVT ensemble for 50 ns with a  
 136 time step of 1 fs. The temperature was controlled by a Nosé–Hoover thermostat<sup>31,32</sup> at 300 K with a time constant  
 137 of 100 fs. The effect of the thermostat on the resultant diffusion constant has been shown to be negligible in these  
 138 conditions<sup>20</sup> for various methods, thus allowing us to get the position-dependent diffusion constant. The total force  
 139 acting on the COM of the methane molecule was sampled every 1 fs. The electrostatic potential was calculated by  
 140 the particle mesh Ewald method with a short-range cutoff length of 1.2 nm. The van der Waals interaction was cut  
 141 off at 1.2 nm and the cutoff correction applied. All simulations were performed using GROMACS 2019<sup>33</sup>, which  
 142 was modified to constrain the methane molecule. The water molecules were modeled by the SPC model<sup>34</sup> and the  
 143 methane molecule was modeled by OPLS-UA<sup>35</sup>.

### 144 3.2 | Analysis

145 We demonstrated numerically the satisfaction of Eq. 14 and thereby the theoretical framework described in the  
 146 aforementioned section. To achieve this, we evaluated  $\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle$  and  $\langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle$ . Given these time cor-  
 147 relation functions, the integrand on the right hand-side of Eq. 14 can be obtained via Eqs. 12 and 15. In partic-  
 148 ular,  $\langle \mathbf{F}_X(0) \cdot \mathbf{v}_{CM}(\tau) \rangle$  was obtained by integrating  $\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle$  from zero to  $\tau$  (see Eq. 15). The time correla-  
 149 tion function  $\langle \mathbf{F}_X(0) \cdot \mathbf{F}_X(t) \rangle$  was evaluated as  $\langle \mathbf{F}^{\text{sim}}(t; \infty) \cdot \mathbf{F}^{\text{sim}}(0; \infty) \rangle$  or the force autocorrelation function obtained  
 150 from the trajectories with  $\tau_{v0} = \infty$ , as these trajectories are the realization of dynamics of the Liouvillian opera-  
 151 tor. As regards the smaller system,  $\langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle$  was calculated from the trajectory with  $\tau_{v0} = 1$  fs, which is a

152 faithful realization of the dynamics defined by Eqs. 16 and 17. In other words,  $\langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle$  was calculated by  
 153  $\langle \mathbf{F}^{\text{sim}}(t; 1 \text{ fs}) \cdot \mathbf{F}^{\text{sim}}(0; 1 \text{ fs}) \rangle$ . For the larger system,  $\langle \mathbf{R}_X(0) \cdot \mathbf{R}_X(t) \rangle$  was substituted by the FACF obtained for  $\tau_{v0} = 0.1$   
 154 ps,  $\langle \mathbf{F}^{\text{sim}}(t; 0.1 \text{ ps}) \cdot \mathbf{F}^{\text{sim}}(0; 0.1 \text{ ps}) \rangle$ , which was found to approximate well the dynamics defined by Eqs. 16 and 17, as  
 155 described in the following section. In these calculations, the numerical integration was performed using the trapezoidal formula.  
 156

## 157 4 | RESULTS AND DISCUSSION

### 158 4.1 | Smaller system

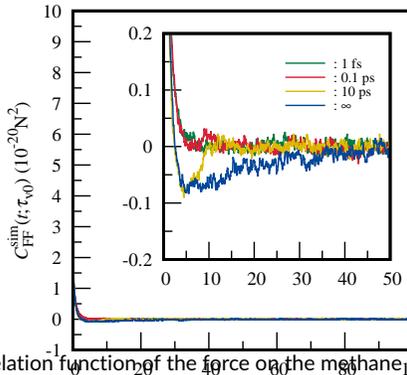


FIGURE 1 Time correlation function of the force on the methane molecule at  $\tau_{v0} = 1 \text{ fs}$  (green),  $0.1 \text{ ps}$  (red),  $10 \text{ ps}$  (yellow), and  $\infty$  (blue) in the smaller system. The inset shows a magnified view for  $0 \leq t \leq 50$  ps.

159 Figure 1 shows time correlation functions of the force on the methane molecule at  $\tau_{v0} = 1 \text{ fs}$ ,  $0.1 \text{ ps}$ ,  $10 \text{ ps}$ , and  
 160  $\infty$  in the smaller system. This graph shows that the time correlation function for  $\tau_{v0} \leq 0.1 \text{ ps}$  converged to zero  
 161 immediately. On the other hand, a negative correlation appears for  $\tau_{v0} \geq 10 \text{ ps}$ . Considering that the absence of the  
 162 negative tail for the systems of  $\tau_{v0} = 1 \text{ fs}$  and  $0.1 \text{ ps}$  can be ascribed to the fast decay of the tail, the larger  $\tau_{v0}$  is, the  
 163 more slowly the negative correlation relaxes. The negative correlation for  $\tau_{v0} = 10 \text{ ps}$  disappears at approximately  $10$   
 164 ps. This means that the effect of the momentum given by the solute to the solvent disappears due to the shift in the  
 165 COM velocity at times longer than  $\tau_{v0}$ . The MB method calculates the diffusion coefficient by

$$D = \frac{3(k_B T)^2}{\int_0^\infty \langle \Delta \mathbf{F}_X(0) \cdot \Delta \mathbf{F}_X(t) \rangle dt}. \quad (23)$$

166 Here,  $\Delta$  is appended to  $\mathbf{F}_X(t)$  to describe explicitly the deviation from the mean force, however,  $\Delta$  can be omitted  
 167 in homogeneous systems as considered in this work. Equation 23 indicates that the diffusion coefficient is inversely  
 168 proportional to the integrated value of FACF. Therefore, the fact that the shape of the time correlation function in  
 169 Fig. 1 differs depending on  $\tau_{v0}$  means that the calculated diffusion coefficient also differs depending on  $\tau_{v0}$ .

170 Figure 2 shows the running integrals of the time correlation functions of the force at  $\tau_{v0} = 1 \text{ fs}$ ,  $0.1 \text{ ps}$ ,  $10 \text{ ps}$ ,

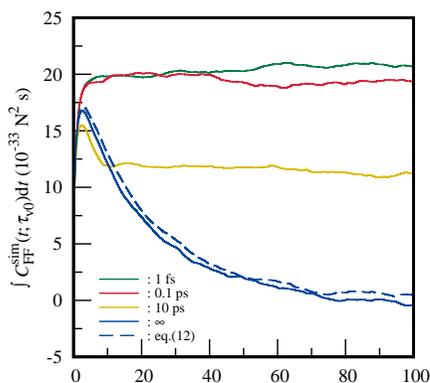


FIGURE 2 Running integrals of the time correlation function of the force on the methane molecule at  $\tau_{v0} = 1$  fs (green), 0.1 ps (red), 10 ps (yellow), and  $\infty$  (blue) in the smaller system. The curve calculated by the right-hand side of Eq. 14 is shown by the blue dashed line.

171 and  $\infty$  in the smaller system. When the time correlation function of the force converges to zero, the integrated  
 172 value converges to a certain value. By substituting this converged value into Eq. 23, the diffusion coefficient can be  
 173 estimated, and Fig. 2 clearly shows that the converged values differ depending on  $\tau_{v0}$ . As mentioned in Section 2, the  
 174 integral converges to the correct value when the COM velocity of the system is removed at every step. Therefore,  
 175 the converged integral value at  $\tau_{v0} = 1$  fs is correct. For  $\tau_{v0} \leq 0.1$  ps, the running integral converged to the same  
 176 value as that at  $\tau_{v0} = 1$  fs. This means that  $\tau_{v0} = 0.1$  ps would be sufficiently small to give accurate results for the size  
 177 of the system in this MD calculation. As  $\tau_{v0}$  increases, the converged value became smaller and smaller, and  $\tau_{v0} = \infty$   
 178 converges to 0, which is consistent with Eq. 18. The physical explanation is that the momentum given by the solute  
 179 to the solvent is finally returned to the solute, because  $\tau_{v0} = \infty$  means the absence of a momentum sink other than  
 180 the solute itself. Moreover, comparing the functional form of the calculation result until it converges to zero with the  
 181 result from the theoretical equation (Eq. 14), the curve at  $\tau_{v0} = \infty$  is consistent with the curve obtained from the  
 182 theoretical equation. Therefore, the numerical calculations support the validity of our theory. The running integral at  
 183  $\tau_{v0} = 10$  ps follows the similar decay at  $t < \tau_{v0}$ , and converges to the finite value at the longer time. In other words,  
 184 the theory elucidates that the diffusion coefficient from the MB method depends on the period ( $\tau_{v0}$ ) in which the  
 185 COM velocity is removed during MD simulations. The theory thus captures the physical mechanism by which the  
 186 choice of  $\tau_{v0}$  affects the FAFs through the modification of the correlation functions.

## 187 4.2 | Larger system

188 Time correlation functions of the force on the methane molecule and their running integrals are shown in Figs. 3 and  
 189 4, respectively, at  $\tau_{v0} = 0.1$  ps, 10 ps, and  $\infty$  in the larger system. Figure 3 shows that the negative correlation is  
 190 weaker than that of the smaller system. As the MD system size increases, the momentum of the system is distributed  
 191 over a larger space, and the COM velocity of the solvent generated by the momentum given by the solute becomes  
 192 smaller. Therefore, the dependence on  $\tau_{v0}$  becomes smaller as the system size of the MD calculations increases. For  
 193  $\tau_{v0} = \infty$ , the negative correlation is weaker than that in the smaller system, but its relaxation becomes slower, as

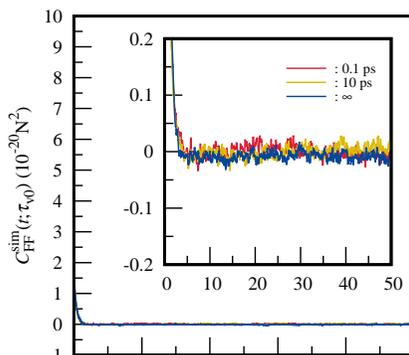


FIGURE 3 Time correlation function of the force on the methane molecule at  $\tau_{v0} = 0.1$  ps (red), 10 ps (yellow), and  $\infty$  (blue) in the large system. The inset shows a magnified view for  $0 \leq t \leq 50$  ps.

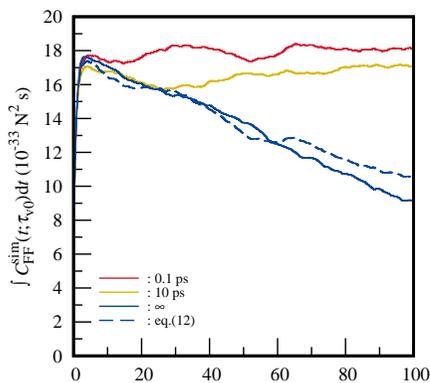


FIGURE 4 Integrating the time correlation functions of the force on the methane molecule at  $\tau_{v0} = 0.1$  ps (red), 10 ps (yellow), and  $\infty$  (blue) in the large system. The curve calculated by Eq. 14 is shown by the blue dotted line.

194 shown in Figure 4. Eq. 18 predicts theoretically that the running integral at  $\tau_{v0} = \infty$  should converge to zero for any  
 195 finite systems, but unlike the smaller system, here the convergence was not complete even at 100 ps. The reason  
 196 for this slow relaxation is that the larger the system, the longer it takes for the momentum to return. The agreement  
 197 between the MD simulation and the theoretical prediction of Eq. 14 is excellent, also in the larger system, Fig. 4,  
 198 which further supports our theoretical discussion. Figure 4 shows that, for the larger system, the result with  $\tau_{v0} = 10$   
 199 ps was close to the correct value ( $\tau_{v0} = 0.1$  ps). Therefore, the larger the system size, the larger  $\tau_{v0}$  can be set.

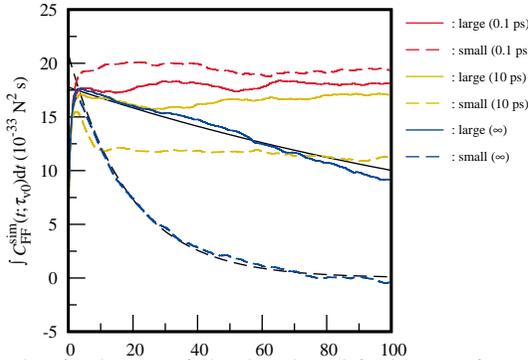


FIGURE 5 Integrating the time correlation function of the force on the methane molecule at  $\tau_{v0} = 0.1$  ps (red), 10 ps (yellow), and  $\infty$  (blue) in the large (solid line) and small (dashed line) systems. Eq. (19) of the large and small systems is shown by black solid and dashed lines.

200 According to Eq. 22, the  $\tau_{FF}$  of the small and large systems were 19.1 and 174.7 ps, respectively. Eq. 21 is plotted  
 201 using these  $\tau_{FF}$  and regarding the amplitude as an adjustable parameter. In addition, the running integrals of the time  
 202 correlation functions of the force on COM of the methane molecule in the larger and smaller systems are shown again  
 203 in Fig. 5 to make their difference clearly visible. It can be seen that Eq. 20 reproduces the decay well at  $\tau_{v0} = \infty$  for  
 204 both the smaller and larger systems.  $\tau_{FF}$  is a reference quantity for determining  $\tau_{v0}$ , and the larger the  $\tau_{FF}$ , the larger  
 205 the value of  $\tau_{v0}$  can be set. The larger the size of the system, the larger the value of  $\tau_{FF}$ , which shows that  $\tau_{v0}$  can be  
 206 larger for larger systems. We mentioned in Section 4.2 that  $\tau_{v0} = 0.1$  ps, which is one two-hundredths of  $\tau_{FF}$ , is small  
 207 enough to calculate  $D$  in the smaller system with sufficient accuracy. It is thus sufficient to set  $\tau_{v0}$  to 1/200th of  $\tau_{FF}$   
 208 even for a small system with fast decay. In the larger system, the result of  $\tau_{v0} = 10$  ps, which is about 1/20th of  $\tau_{FF}$   
 209 of the system, is close to that of  $\tau_{v0} = 0.1$  ps. Therefore, it is safe to set  $\tau_{v0}$  to at most 1/200th of  $\tau_{FF}$  for any system  
 210 larger than the smaller system.

211 For  $\tau_{v0} \geq 10$  ps, the integral was larger for the larger system than that for the smaller one, indicating that the  
 212 larger the size of the system, the longer the time part was affected, as discussed previously. However, at  $\tau_{v0} = 0.1$   
 213 ps, the integral of the smaller system was larger than that of the larger system. This is not an effect of the shift of  
 214 the COM velocity, but that of the hydrodynamic interaction between the solutes in adjacent cells in the periodic  
 215 boundary system. Due to the effects of hydrodynamic interaction, the diffusion coefficient,  $D_{MD}$ , calculated from the  
 216 MD calculation of the finite system with periodic boundary conditions, is shifted from the true diffusion coefficient

217  $D_0$  of the system of infinite size as shown in the following equation<sup>36</sup>:

$$D_{MD} = D_0 - \frac{2.83729k_B T}{6\pi\mu L} \quad (24)$$

218 where  $\mu$  and  $L$  are the viscosity coefficient and the length of the MD cell, respectively. This equation states that  
 219 the smaller the cell size, the smaller  $D_{MD}$  becomes. Since the integral value of the time correlation function of the  
 220 force is the reciprocal of  $D_{MD}$  (see Eq. 23), it becomes larger for smaller systems. Using the experimental viscosity  
 221 coefficient of water at 25 °C ( $\mu = 0.0009$  Pa·s) and Eq. 24, the difference in the integrated values of the time correlation  
 222 functions of the force between the larger and the smaller systems was calculated to be  $1 \times 10^{-10} \text{ m}^2 \cdot \text{s}^{-1}$ . On the  
 223 other hand, the difference found from our calculation, shown in Fig.5, is  $2 \times 10^{-10} \text{ m}^2 \cdot \text{s}^{-1}$ . So, the estimates from  
 224 the theoretical equations of fluid mechanics and our calculation are in good agreement, considering the error guessed  
 225 from the fluctuation of the running integral.

### 226 4.3 | Relevance to NVE ensemble and other thermostats

227 The formalized theory perfectly fits with the NVE ensemble, and thus the COM velocity shift is needed to eliminate  
 228 the unwanted negative correlation between  $\mathbf{F}(0)$  and  $\mathbf{F}(t)$ . However, the shift decreases the total energy when applied  
 229 to the NVE simulations and therefore the simulations cannot reach thermal equilibrium. Furthermore, this decrease  
 230 can cause a drop in the temperature and thus the diffusion constant can be underestimated. It should be carefully  
 231 confirmed that the drift of the total energy or temperature is so marginal that the potential systematic error is satis-  
 232 factorily small in application to NVE simulations. Given this potential artifact that is intrinsic to the NVE simulations,  
 233 the coupling of a thermostat should be a practical choice, especially for long simulations, although disturbance from  
 234 a thermostat to the original dynamics needs to be carefully considered. We have performed NVT simulations using a  
 235 Nosé–Hoover thermostat in this work, and demonstrated that the discussion based on the NVE ensemble holds. We  
 236 next discuss the applicability of the COM velocity shift to thermostats other than the Nosé–Hoover thermostat. Other  
 237 widely used thermostats include the Gaussian constraint<sup>37–40</sup>, velocity rescaling<sup>41</sup>, and a Langevin thermostat<sup>29</sup>.

238 A COM velocity shift is necessary for the thermostats that retain linear momentum conservation, such as the  
 239 Gaussian constraint<sup>37–40</sup> and velocity rescaling<sup>41</sup>, because the unwanted negative correlation between  $\mathbf{F}(0)$  and  $\mathbf{F}(t)$   
 240 arises ultimately from the momentum conservation (Eq. 7) in a finite system as described above. Furthermore, we  
 241 have demonstrated numerically the necessity of the COM velocity shift for the Nosé–Hoover thermostat, which also  
 242 retains the momentum conservation. When it comes to thermostats that break the momentum conservation, including  
 243 the Langevin thermostat, we need to give more subtle consideration as follows.

244 When applying the Langevin thermostat, the coupling time constant  $\tau_{LT}$  ( $\tau_{LT} \equiv 1/\gamma$ , where  $\gamma$  is the damping  
 245 coefficient of the thermostat) needs to be considered, as the thermostat works also as the momentum sink with this  
 246 time constant  $\tau_{LT}$ . If the coupling is sufficiently strong, i.e.,  $\tau_{LT} \ll \tau_{FF}$ , the diminishing behavior of the running integral  
 247 of  $\langle \mathbf{F}_X(t) \cdot \mathbf{F}_X(0) \rangle$  should not be observed, because the COM momentum drops quickly. Nevertheless, because such  
 248 a strong coupling might disturb the short-term dynamics as well, the potential artifact in the diffusion constant should  
 249 be considered carefully. If the coupling is weak such that  $\tau_{LT} \gg \tau_{FF}$ , the running integral of  $\langle \mathbf{F}_X(t) \cdot \mathbf{F}_X(0) \rangle$  should  
 250 diminish, as the momentum drops too slowly. In this case, the COM velocity shift should be performed frequently  
 251 enough such that  $\tau_{v0} \ll \tau_{FF}$ , even with this thermostat.

## 4.4 | Discussion on how to constrain the solute

### 4.4.1 | Harmonic constraint

The WR method is another popular method for evaluating the position-dependent diffusion coefficient<sup>12</sup>. In the WR method, the solute is constrained around a position of interest by a harmonic potential, and the spring constant of the potential,  $k$ , is an adjustable parameter. We hereafter discuss how the COM velocity shift of the solvent affects the diffusion coefficient when the solute is constrained to absolute coordinates in the WR method. For simplicity, we consider a homogeneous system where no potential of mean force is induced on the solute by the solvent. When the system size is infinite, the dynamics of the solute in the WR method is described by the generalized Langevin equation as

$$\dot{\mathbf{r}}_X(t) = \mathbf{v}_X(t), \quad (25)$$

$$m_X \dot{\mathbf{v}}_X(t) = \mathbf{F}_X(t), \quad (26)$$

$$\mathbf{F}_X(t) = \mathbf{R}_X(t) - \int_0^t d\tau \gamma(t-\tau) \mathbf{v}_X(\tau) - k \mathbf{r}_X(t). \quad (27)$$

Here, the mass, position, and velocity of the solute are denoted as  $m_X$ ,  $\mathbf{r}_X(t)$ , and  $\mathbf{v}_X(t)$ , respectively, and the solute is assumed to be constrained to the origin. The equations above are solved to yield the time correlation function of the position as

$$\int_0^\infty dt \langle \mathbf{r}_X(0) \cdot \mathbf{r}_X(t) \rangle = \frac{\tilde{\gamma}_0}{k} \langle |\mathbf{r}_X(0)|^2 \rangle, \quad (28)$$

$$\tilde{\gamma}_0 \equiv \int_0^\infty dt \gamma(t). \quad (29)$$

For derivation, readers refer to, e.g., Refs. 12,13,27,42 and also Sec. S2 of Supporting Information. Substituting the relationship between the fluctuation of the position and  $k$  as

$$\langle |\mathbf{r}_X(0)|^2 \rangle = \frac{3k_B T}{k}, \quad (30)$$

the diffusion coefficient is determined by the equation as follows:

$$D = \frac{k_B T}{\tilde{\gamma}_0} = \frac{\langle |\mathbf{r}_X(0)|^2 \rangle^2}{3 \int_0^\infty dt \langle \mathbf{r}_X(0) \cdot \mathbf{r}_X(t) \rangle}. \quad (31)$$

We would like to note that Eq. 23 holds for finite  $k$  values<sup>27</sup> and that the diffusion constant obtained by Eq. 31 theoretically equals that obtained by Eq. 23.

Next we consider the finite-size system, to which the shift of the COM velocity of the solvent is applied with a time interval of  $\tau_{v0}$ . Then, Eqs. 25 and 26 are intact, and Eq. 27 is modified as

$$\mathbf{F}_X(t) = \mathbf{R}_X(t) - \int_0^t d\tau \gamma(t-\tau) (\mathbf{v}_X(\tau) - \mathbf{v}_{CM}(\tau)) - k \mathbf{r}_X(t), \quad (32)$$

$$M_S \dot{\mathbf{v}}_{CM}(t) = -[\mathbf{F}_X(t) + k \mathbf{r}_X(t)] - \gamma_s M_S \mathbf{v}_{CM}(t). \quad (33)$$

Here, the shift of the COM velocity is approximated as the damping with a time constant of  $\tau_{v0} = 1/\gamma_s$ . The time

272 correlation function of the position is then obtained from Eqs. 25, 26, 32, and 33 as

$$\int_0^{\infty} dt \langle r_X(0) \cdot r_X(t) \rangle = \frac{\tilde{\gamma}_0}{k \left( 1 + \frac{\tilde{\gamma}_0}{M_S \gamma_s} \right)} \langle |r_X(0)|^2 \rangle, \quad (34)$$

273 whose derivation is described in Sec. S2 of Supporting Information. Comparing Eqs. 28 and 34, it is shown that the  
274 WR method gives the correct value of the diffusion coefficient under the condition as

$$\tau_{v0} = \frac{1}{\gamma_s} \ll \frac{M_S}{\tilde{\gamma}_0}, \quad (35)$$

275 which is the same condition as the MB method.

276 It is rather surprising that the condition Eq. 35 does not contain  $k$ . One may consider that  $\tau_{v0}$  can be smaller  
277 with decreasing  $k$ , because the diffusion coefficient from the WR method reduces to that from the mean square  
278 displacement of the unconstrained solute, for which the shift of the COM velocity is unnecessary. However, Eq. 35  
279 means that the removal of the COM velocity is indispensable in the WR method, irrespective of the strength of the  
280 constraining potential. The result above indicates that the COM velocity of the solvent should be removed with  
281 sufficient frequency when the solute is constrained to absolute coordinates, irrespective of how the constraint is  
282 performed.

#### 283 4.4.2 | Constraint by relative coordinates

284 Instead of constraining to absolute coordinates, it is also common to constrain the relative coordinates of two sub-  
285 stances in order to calculate the position-dependent diffusion coefficients in heterogeneous systems. For example,  
286 membrane permeation<sup>43</sup> or substrate adsorption<sup>44</sup> of small molecules, and the transport across a transmembrane  
287 channel of ions<sup>45</sup> are all discussed in terms of potential mean force (PMF) and the position-dependent relative diffu-  
288 sion coefficient between two substances such as a membrane and a molecule.

289 In this case, external forces do not work, and only internal forces do. Therefore, momentum does not flow to-  
290 ward the solvent, and the error discussed in this paper does not occur. Therefore,  $\tau_{v0}$  can be determined solely by  
291 considering its original purpose to compensate the numerical errors in the Ewald calculation.

## 292 5 | CONCLUSION

293 It was shown theoretically that the position-dependent diffusion coefficient obtained using the MB method depends  
294 on  $\tau_{v0}$ . For systems as small as 1000 molecules, the FACF integrals converge well at  $\tau_{v0} \leq 0.1$  ps, indicating that the  
295 diffusion coefficient can be obtained with good accuracy. However, at  $\tau_{v0} \geq 10$  ps, the integral converges to a value  
296 different from the correct one. The larger was  $\tau_{v0}$ , the smaller the converged value of the FACF integral became. The  
297 converged value was zero at  $\tau_{v0} = \infty$ , which has good consistency with the theoretical prediction, thereby supporting  
298 the validity of our theory.

299 For a system as large as 8000 molecules, the converged value of the FACF integral was close to the correct one  
300 even when  $\tau_{v0}$  was as large as 10 ps. In addition, the convergence of the integrated value became slower at  $\tau_{v0} = \infty$ .  
301 This result is also consistent with our theoretical prediction, and shows that our theory is applicable, irrespective of  
302 the system size. These calculations demonstrate the necessity of choosing  $\tau_{v0}$  according to the size of the system  
303 when calculating the position-dependent diffusion coefficient by the MB method using MD calculation with the Ewald

304 method. From the point of view of the speed of MD calculation, removing the COM velocity of the system requires  
305 full communication between nodes of parallel computers, which slows down the calculation speed. Therefore,  $\tau_{v0}$  is  
306 preferred to be as large as possible, but 0.1 ps is probably sufficient for ordinary systems.

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## 313 Data Availability Statement

314 The data that support the findings of this study are available from the corresponding author upon reasonable request.

## 315 Supporting Information

316 Additional Supporting Information may be found in the online version of this article.

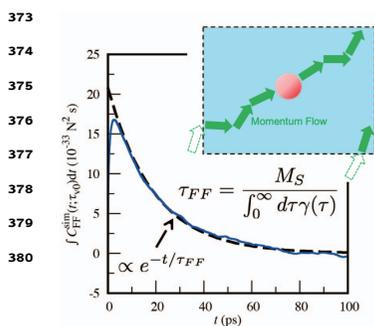
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## 372 GRAPHICAL ABSTRACT



The position-dependent diffusion coefficient is beneficial for studying mass transport with molecular dynamics calculations. In the Marrink–Berendsen method, this coefficient can be obtained from the integral of force autocorrelation function of a fixed molecule at an absolute position. However, the integrated values evaluated so in a finite system diminishes due to momentum flows arising from momentum conservation, and the diffusion coefficient diverges unphysically. We rigorously demonstrate that frequent removals of total momentum eliminate this flaw.