

A SOLUTION OF THE EQUATIONS OF MOTION OF VISCOUS FLUID FOR DIMINISHING VISCOSITY

ZUYURÔ SAKADI and EIITI TAKIZAWA

Department of Dynamics

(Received April 30th, 1949)

I. Introduction

The 2-dimensional problem of the Oseen's linearized equations of stationary motion of viscous fluid around a cylindrical solid body for the limiting case viscosity $\rightarrow 0$, was reduced by Oseen into the following results. (Oseen, *Hydrodynamik, Mathematik in Monographien und Lehrbüchern*).

Let

- $x_j (j = 1, 2)$: rectangular coordinates,
- $U (> 0)$: constant velocity of fluid for $x_1^2 + x_2^2 \rightarrow \infty$ in the x_1 negative direction,
- $u_1 - U, u_2$: components of velocity,
- p : pressure,
- ρ : density,
- B_v : the region of fluid which is not passed by the solid body,
- B_h : the region which is passed by the body,
- S_v : the surface of the body facing to B_v ,
- S_h : the surface of the body facing to B_h .

Then the results are :

in B_v : $u_j = v_j, \quad (j = 1, 2),$

in B_h : $u_1 = v_1 - (v_1)_h + U, \quad u_2 = v_2,$

and in both regions

$$p = \rho U v_1 - \frac{1}{2} \rho (u_1^2 + u_2^2),$$

where $(v_1)_h =$ value of v_1 on S_h with same x_2 , and v_1 and v_2 are to be determined in the following way.

Let

$$x_1 + ix_2 = z,$$

$z = f(z')$: conformal representation of the outer region of $S = S_v + S_h$ into $|z'| > 1$ so that the boundary S_v is represented by $z' = z^* = e^{i\theta^*}, -\frac{\pi}{2} < \theta^* < \frac{\pi}{2}$ and S_h by $\frac{\pi}{2} < \theta^* < \frac{3}{2}\pi$ respectively.

Put

$$\infty = f(z'_0),$$

and make

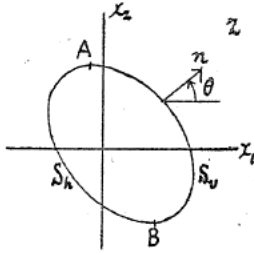


Fig. 1 a.

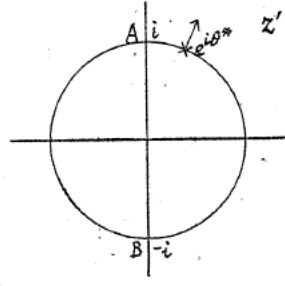


Fig. 1 b.

$$w(z') = \frac{1}{\pi} \int_{\theta^* = -\pi/2}^{\pi/2} \left(\theta(\theta^*) - \frac{\pi}{2} \right) \left(\frac{1}{z^* - z'} - \frac{1}{2z^*} \right) dz^*, \dots\dots\dots (I, 1)$$

where

$$\theta(\theta^*) = \text{arc}(n, x_1), \quad z^* = e^{i\theta^*},$$

n : outward normal to S_v at $z = f(e^{i\theta^*})$,

and

$$-\frac{\pi}{2} < \theta(\theta^*) < \frac{\pi}{2} \quad \text{for} \quad -\frac{\pi}{2} < \theta^* < \frac{\pi}{2}.$$

Further put

$$W(z') = U + e^{w(z')} \cdot \left(k_1 + ik_2 \frac{z' - i}{z' + i} \right), \dots\dots\dots (I, 2)$$

where the real constants k_1, k_2 are to be determined by

$$W(z'_0) = 0.$$

Finally we obtain

$$W(z') = W(z) = v_1 - iv_2. \dots\dots\dots (I, 3)$$

The resistance and lift on the body can be calculated by the formulas

$$-\frac{1}{2} \rho \int_{S_h} (U - v_1)^2 dx_2, \dots\dots\dots (I, 4)$$

$$2\pi B \rho U^2 - \frac{1}{2} \rho \int_{S_h} (U^2 - v_1^2) dx_1, \dots\dots\dots (I, 5)$$

respectively, where the integration must be taken in positive sense along S_h and B is determined by

$$W(z) = U \frac{A - iB}{z} + \dots\dots\dots (I, 6)$$

The calculation of this problem has been carried out, as far as we know, in the following 2 cases: the curve $S = S_v + S_h$ is a circle or a line segment. We treat in this paper the lens-shaped case.

II. Conformal Representation and the Determination of $w(z')$ and $W(z')$

We take the 2 side curves of the cross section as arcs of circles and put the cross section as is shown in Fig. 2.

$$0 < \gamma \leq \frac{\pi}{2},$$

$$-\gamma \leq \beta \leq \alpha \leq \gamma.$$

The conditions that the arcs ACB and ADB shall be S_v and S_h respectively are fulfilled.

We transform the z -plane successively by

$$\zeta = e^{i(\pi/2 - \gamma)} z,$$

$$\xi = \frac{\zeta + i}{\zeta - i} \quad \left(\zeta = i \frac{\xi + 1}{\xi - 1} \right),$$

$$u = \xi^{\pi/(2\pi - (\alpha - \beta))},$$

$$v = e^{i\delta} u,$$

$$\delta = \frac{\pi}{2} - (\pi - \alpha) \frac{\pi}{2\pi - (\alpha - \beta)} = \frac{1}{\varepsilon} \frac{\alpha + \beta}{2},$$

$$\varepsilon = 2 - \frac{1}{\pi} (\alpha - \beta),$$

$$z' = i \frac{v + 1}{v - 1} \quad \left(v = \frac{z' + i}{z' - i} \right).$$

$$z'_0 = \operatorname{ctg} \frac{\delta}{2}.$$

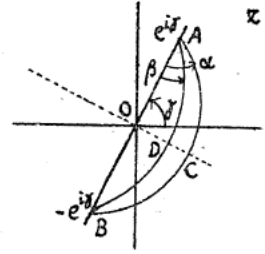


Fig. 2.

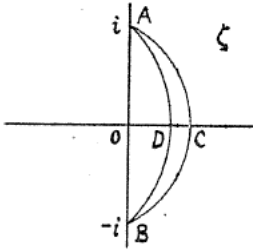


Fig. 3 a.

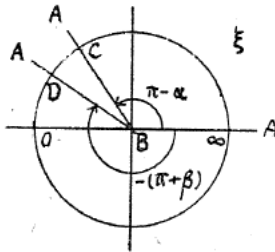


Fig. 3 b.

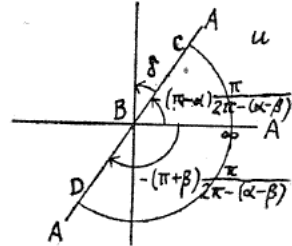


Fig. 3 c.

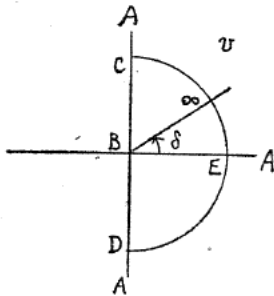


Fig. 3 d.

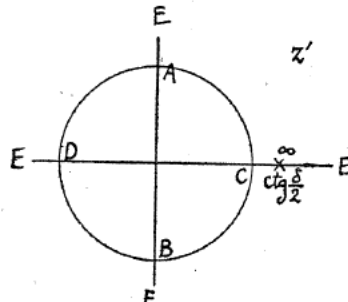


Fig. 3 e.

Calculation of $\theta(\theta^*)$.

In the ζ -plane let the center of the arc ACB be $O_1(-\operatorname{ctg} \alpha)$, (the radius $= \frac{1}{|\sin \alpha|}$) then for ζ on the arc we have:

$$\zeta - (-\operatorname{ctg} \alpha) = \frac{1}{\sin \alpha} e^{i\theta_1}, \quad \dots \dots \dots (\text{II}, 1)$$

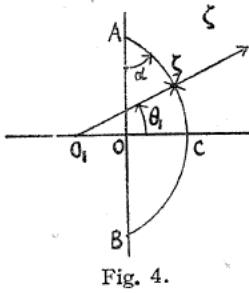


Fig. 4.

and

$$\theta(\theta^*) = \theta_1(\theta^*) - \left(\frac{\pi}{2} - \gamma\right),$$

$$z' = z^* = e^{i\theta^*},$$

$$v = \frac{z^* + i}{z^* - i} = e^{(\pi/2)i} \operatorname{ctg}\left(\frac{\pi}{4} - \frac{\theta^*}{2}\right),$$

$$\xi = e^{(\pi/2 - \delta)\varepsilon i} \left\{ \operatorname{ctg}\left(\frac{\pi}{4} - \frac{\theta^*}{2}\right) \right\}^\varepsilon = e^{(\pi - \alpha)i} \cdot \left\{ \operatorname{ctg}\left(\frac{\pi}{4} - \frac{\theta^*}{2}\right) \right\}^\varepsilon.$$

Hence combining with (II, 1)

$$\zeta = i \frac{-e^{\alpha i} (\operatorname{ctg})^\varepsilon + 1}{-e^{-\alpha i} (\operatorname{ctg})^\varepsilon - 1} = \frac{e^{i\theta_1} - \cos \alpha}{\sin \alpha},$$

$$e^{i\theta_1} = \frac{(\operatorname{ctg})^\varepsilon + e^{-i\alpha}}{(\operatorname{ctg})^\varepsilon + e^{i\alpha}} e^{i\alpha} = e^{-2i\varphi + i\alpha}, \quad (\text{II, 2}) \quad \theta_1 = \alpha - 2\varphi,$$

with

$$0 \leq \frac{\varphi}{\alpha} \leq 1.$$

From (II, 2) or directly from the symmetry of the representation ($\zeta \rightarrow z'$) it is clear that

$$\theta_1(-\theta^*) = -\theta_1(\theta^*).$$

From (I, 1) regarding (II, 3) we obtain:

$$\begin{aligned} w(z') &= \frac{\gamma - \pi}{\pi} \int \left(\frac{1}{z^* - z'} - \frac{1}{2z^*} \right) dz^* + \frac{1}{\pi} \int \theta_1(\theta^*) \left(\frac{1}{z^* - z'} - \frac{1}{2z^*} \right) dz^* \\ &= \frac{\gamma - \pi}{\pi} \operatorname{lg} \frac{z' - i}{z' + i} - \frac{i}{2} (\gamma - \pi) + \frac{1}{\pi} \int \theta_1(\theta^*) \frac{dz^*}{z^* - z'}, \\ e^{w(z')} &= ie^{-i\gamma/2} \cdot \left(\frac{z' + i}{z' - i} \right)^{1 - (\gamma/\pi)} \cdot e^{a(z')}, \end{aligned}$$

where

$$a(z') = \frac{1}{\pi} \int \theta_1(\theta^*) \frac{dz^*}{z^* - z'} = \frac{2}{\pi} z' \int_0^{\pi/2} \theta_1(\theta^*) \frac{\sin \theta^* d\theta^*}{z'^2 - 2z' \cos \theta^* + 1}, \quad \dots \dots (\text{II, 4})$$

and

$$a(z'_0) = a\left(\operatorname{ctg} \frac{\delta}{2}\right) = a_0 : \text{real}.$$

We put

$$1 - \frac{\gamma}{\pi} = \eta, \quad \delta + \frac{\pi}{2} = \frac{\pi + \beta}{\varepsilon} = \omega,$$

then

$$e^{w(z'_0)} = e^{i\eta\omega} \cdot e^{a_0},$$

and by the condition

$$W(z'_0) = 0$$

we have

$$\left. \begin{aligned} k_1 &= -\frac{\sin(1 - \eta)\omega}{\sin \omega} e^{-a_0} \cdot U, \\ k_2 &= \frac{\sin \eta\omega}{\sin \omega} e^{-a_0} \cdot U. \end{aligned} \right\} \dots \dots (\text{II, 5})$$

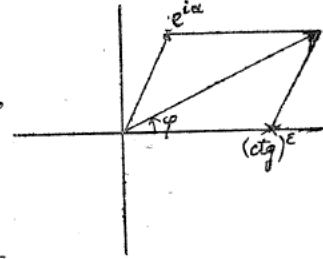


Fig. 5.

.....(II, 3)

Hence we have:

$$\begin{aligned}
 W(z') &= U \left\{ 1 - \frac{e^{-a_0}}{\sin \omega} e^{i\omega(z')} \left[\sin(1 - \eta)\omega - i \sin \eta\omega \cdot \frac{z' - i}{z' + i} \right] \right\} \\
 &= U \left\{ 1 - \frac{e^{a-a_0}}{\sin \omega} e^{i\eta\pi/2} v^\eta \left[\sin(1 - \eta)\omega - i \sin \eta\omega \cdot \frac{1}{v} \right] \right\}. \dots\dots\dots (II, 6)
 \end{aligned}$$

We expand (II, 6) as a function of z in power series of $\frac{1}{z}$.

$$\begin{aligned}
 \xi &= 1 + \frac{2i}{\zeta} + \dots, \\
 u &= 1 + \frac{2i}{\varepsilon} \frac{1}{\zeta} + \dots, \quad v = e^{i\delta} \left(1 + \frac{2i}{\varepsilon} \frac{1}{\zeta} + \dots \right), \\
 z' &= \operatorname{ctg} \frac{\delta}{2} - \frac{1}{\varepsilon \sin^2 \frac{\delta}{2}} \cdot \frac{1}{\zeta} + \dots = \operatorname{ctg} \frac{\delta}{2} + \frac{ie^{i\tau}}{\varepsilon \sin^2 \frac{\delta}{2}} \frac{1}{z} + \dots, \\
 a &= a_0 + \frac{2}{\varepsilon} \frac{ie^{i\tau}}{\pi \sin^2 \frac{\delta}{2}} \frac{1}{z} \int_0^{\pi/2} \theta_1(\theta^*) \sin \theta^* d\theta^* \times \\
 &\quad \times \left\{ \frac{1}{z'^2 - 2z' \cos \theta^* + 1} + z' \frac{\partial}{\partial z'} \frac{1}{z'^2 - 2z' \cos \theta^* + 1} \right\}_{z' = \operatorname{ctg} \frac{\delta}{2}} \\
 &= a_0 + \frac{2}{\varepsilon} ie^{i\tau} \frac{a_1}{z} + \dots,
 \end{aligned}$$

with

$$\begin{aligned}
 a_0 &= \frac{\sin \delta}{\pi} \int_0^{\pi/2} \frac{\theta_1(\theta^*) \sin \theta^* d\theta^*}{1 - \cos \theta^* \sin \delta}, \\
 a_1 &= -\frac{\cos \delta}{\pi} \int_0^{\pi/2} \theta_1(\theta^*) \frac{\sin \theta^* d\theta^*}{(1 - \cos \theta^* \sin \delta)^2}, \quad (a_1 : \text{real}), \\
 e^{i\omega(z')} &= e^{i\omega(z'_0)} \left[1 + \frac{2}{\varepsilon} e^{i\tau} \left\{ \left(1 - \frac{\tau}{\pi} \right) + ia_1 \right\} \frac{1}{z} + \dots \right], \\
 \frac{W(z)}{U} &= \frac{2}{\varepsilon} e^{-i\eta\pi} \left\{ \eta - \frac{\sin \eta\omega}{\sin \omega} e^{-i(1-\eta)\omega} + ia_1 \right\} \frac{1}{z} + \dots \\
 &= \frac{A - iB}{z} + \dots, \\
 A &= \frac{2}{\varepsilon} \left\{ \eta \cos \eta\pi - \frac{\sin \eta\omega}{\sin \omega} \cos(\eta\omega - \omega - \eta\pi) + a_1 \sin \eta\pi \right\}, \\
 B &= \frac{2}{\varepsilon} \left\{ \eta \sin \eta\pi + \frac{\sin \eta\omega}{\sin \omega} \sin(\eta\omega - \omega - \eta\pi) - a_1 \cos \eta\pi \right\}. \dots\dots\dots (II, 7)
 \end{aligned}$$

A and B determine, in one sense, the radial outflow and circulation.

III. Resistance and Lift on the Solid

When z moves in the z -plane along the arc ADB we get

$$\begin{aligned}
 dz &= e^{-i(\pi/2 - \tau)} d\zeta, \\
 d\zeta &= \frac{-2i}{(\xi - 1)^2} d\xi = \frac{-2i \varepsilon e^{i\varepsilon\delta}}{(v^\varepsilon - e^{i\varepsilon\delta})^2} v^\varepsilon \frac{dv}{v}, \\
 dz &= 2e^{-i\eta\pi} \frac{e^{i\varepsilon\omega}}{(y - e^{i\varepsilon\omega})^2} dy \dots\dots\dots (III, 1)
 \end{aligned}$$

by putting

$$v = e^{-i\pi/2} y^{1/\varepsilon}, \quad (y: +\infty \longrightarrow +0),$$

and from (II, 6)

$$W(z) = U \left\{ 1 - \frac{e^{a-a_0}}{\sin \omega} [\sin(1-\eta)\omega \cdot y^{\eta/\varepsilon} + \sin \eta\omega \cdot y^{(\eta-1)/\varepsilon}] \right\}. \quad \dots (III, 2)$$

Here we see from (I, 3) by putting $v_2 = 0$ or from (III, 2) and (II, 4) that W is real along S_h .

By (I, 4) and (I, 5) we have to calculate:

$$\left. \begin{aligned} -\int_{S_h} (U - v_1)^2 dx_2 &= -\int (U - W)^2 dx_2 = -\Im \int (U - W)^2 dz, \\ \text{and} \\ -\int (U^2 - v_1^2) dx_1 &= -\Re \int (U^2 - W^2) dz \\ &= \Re \int (U - W)^2 dz - 2U \Re \int (U - W) dz. \end{aligned} \right\} \dots (III, 3)$$

Using (III, 1) and (III, 2) we get:

$$\left. \begin{aligned} \int (U - W)^2 dz &= \frac{2U^2 e^{-i(\eta\pi - \varepsilon\omega)}}{\sin^2 \omega} \int_{\infty}^0 \frac{e^{2(a-a_0)}}{(y - e^{i\varepsilon\omega})^2} \times \\ &\quad \times \{ \sin^2(1-\eta)\omega \cdot y^{2\eta/\varepsilon} + 2\sin(1-\eta)\omega \cdot \sin \eta\omega \cdot y^{(2\eta-1)/\varepsilon} + \sin^2 \eta\omega \cdot y^{(2\eta-2)/\varepsilon} \} dy, \\ U \int (U - W) dz &= \frac{2U^2}{\sin \omega} e^{-i(\eta\pi - \varepsilon\omega)} \cdot \int_{\infty}^0 \frac{e^{a-a_0}}{(y - e^{i\varepsilon\omega})^2} \times \\ &\quad \times \{ \sin(1-\eta)\omega \cdot y^{\eta/\varepsilon} + \sin \eta\omega \cdot y^{(\eta-1)/\varepsilon} \} dy. \end{aligned} \right\} \dots (III, 4)$$

Behaviour of e^{α} for $y=0$ and $y=\infty$.

When $z^* = e^{i\theta^*}$ lies on the arc ACB of the z' -plane and is near to A , we have:

$$\begin{aligned} z' &= z^* = i + t, \\ v &= \frac{2i+t}{t} = \frac{2i}{t} \left(1 + \frac{t}{2i} \right), \\ u &= e^{i(\pi/2-\delta)} \cdot \frac{2}{t} \left(1 + \frac{t}{2i} \right), \\ \xi &= e^{i(\pi-\alpha)} \cdot \frac{2^\varepsilon}{t^\varepsilon} \left(1 + \frac{\varepsilon}{2i} t + \dots \right), \\ \zeta &= i(1 - e^{i\alpha} \cdot 2^{1-\varepsilon} t^\varepsilon + \dots), \end{aligned}$$

and by (II, 1)

$$\begin{aligned} e^{i\theta_1} &= \sin \alpha \cdot (\zeta + \operatorname{ctg} \alpha) = e^{i\alpha} (1 - i \sin \alpha \cdot 2^{1-\varepsilon} t^\varepsilon + \dots), \\ \theta_1(\theta^*) &= \alpha + \frac{1}{i} \lg (1 - i \sin \alpha \cdot 2^{1-\varepsilon} t^\varepsilon + \dots) \\ &= \alpha - \sin \alpha \cdot 2^{1-\varepsilon} (z^* - i)^\varepsilon + \dots, \\ &\quad (1 \leq \varepsilon \leq 2). \end{aligned}$$

This last result can also be obtained from (II, 2), and we see from (II, 4) easily that

$$a(z') = \frac{\alpha}{\pi} \cdot \lg(z' - i) + \text{bounded function},$$

when z' is on the arc ADB and near to A . Similarly when z' is on the arc ADB and near to B we have

$$a(z') = \frac{\alpha}{\pi} \lg(z' + i) + \text{bounded function}.$$

Hence we have:

$$e^a = \begin{cases} y^{-\alpha/(\varepsilon\pi)} \cdot F(y), & \text{when } y : \text{real and } y \rightarrow +\infty, \\ y^{\alpha/(\varepsilon\pi)} \cdot F(y), & \text{when } y : \text{real and } y \rightarrow +0, \end{cases}$$

where $F(y)$ represents functions with F and $\frac{1}{F}$ bounded, and e^a is bounded in the other part of the line $y = \text{real positive}$ in the y -plane.

Conditions for convergence of integrals in (III, 4).

The integrals in (III, 4) are of the form:

$$I_{s,k} = \int_{\infty}^0 \frac{e^{s(a-a_0)} y^{(s\eta-k)/\varepsilon}}{(y - e^{i\varepsilon\omega})^2} dy, \quad \dots\dots\dots \text{(III, 5)}$$

with

$$\begin{aligned} s = 1, \quad k = 0, 1, \\ \text{or} \quad s = 2, \quad k = 0, 1, 2. \end{aligned}$$

The condition of convergence of (III, 5) in the neighbourhood of $y = 0$, that is, in the neighbourhood of B in the z -plane is

$$\frac{2(\eta - 1)}{\varepsilon} + \frac{2\alpha}{\varepsilon\pi} > -1, \quad \dots\dots\dots \text{(III, 6)}$$

and that in the neighbourhood of $y = \infty$ (A in z -plane) is

$$\frac{2\eta}{\varepsilon} - \frac{2\alpha}{\varepsilon\pi} < 1. \quad \dots\dots\dots \text{(III, 7)}$$

(III, 6) and (III, 7) can be written in the form

$$\begin{aligned} (\gamma - \alpha) + (\gamma - \beta) < 2\pi, \\ (\gamma + \alpha) + (\gamma + \beta) > 0, \end{aligned}$$

respectively, that is, the first is satisfied except for

$$\left. \begin{aligned} -\alpha = -\beta = \gamma = \frac{\pi}{2}, \\ -\alpha = -\beta = \gamma > 0. \end{aligned} \right\} \dots\dots\dots \text{(III, 8)}$$

and the second except for

These 2 exceptional cases are shown in Fig. 6.

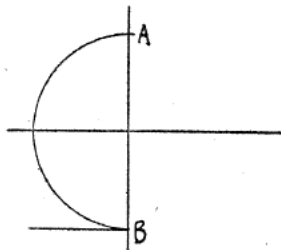


Fig. 6 a.

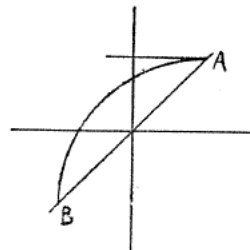


Fig. 6 b.

Calculation of (III, 5) for the case $\alpha = 0$.

Because of the factor $e^{s(a-a_0)}$, which is identically = 1 for $\alpha = 0$, it seems difficult to evaluate (III, 5) in the general case.

When $\alpha = 0$ the exceptional cases (III, 8) do not occur and (III, 5) becomes simply

$$I_k = \int_{-\infty}^0 \frac{y^k}{(y - e^{i\varepsilon\omega})^2} dy, \quad k = \frac{2\eta}{\varepsilon}, \frac{2\eta-1}{\varepsilon}, \frac{2(\eta-1)}{\varepsilon}, \frac{\eta}{\varepsilon}, \frac{\eta-1}{\varepsilon},$$

$$\frac{\pi}{2} \leq \varepsilon\omega = \pi + \beta \leq \pi.$$

To evaluate I_k we put

$$I = \int_{\mathcal{C}} \frac{y^k}{(y - e^{i\varepsilon\omega})^2} dy = (1 - e^{i2k\pi}) \cdot I_k$$

and by method of residue we obtain:

$$I = -i2k\pi e^{i(k-1)\varepsilon\omega},$$

$$e^{-i\eta\pi + i\varepsilon\omega} \cdot I_k = \frac{k\pi e^{i(k\varepsilon\omega - k\pi - \eta\pi)}}{\sin k\pi}.$$

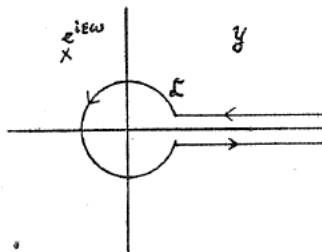


Fig. 7.

Inserting these values into (III, 4) we have the results:

$$\int (U - W)^2 dz = \frac{2U^2}{\sin^2 \omega} \left\{ \sin^2 (1 - \eta) \omega \frac{2\eta(\pi - \omega)}{\sin 2\eta(\omega)} e^{i\eta(4\omega - 3\pi)} - \right.$$

$$\left. - 2 \sin (1 - \eta) \omega \sin \eta\omega \frac{(2\eta - 1)(\pi - \omega)}{\sin (2\eta - 1)(\omega)} e^{i\eta(4\omega - 3\pi) - i2\omega} + \right.$$

$$\left. + \sin^2 \eta\omega \frac{2(\eta - 1)(\pi - \omega)}{\sin 2(\eta - 1)(\omega)} e^{i\eta(\omega) - i4\omega} \right\},$$

$$U \int (U - W) dz = \frac{2U^2}{\sin \omega} \left\{ \sin (1 - \eta) \omega \frac{\eta(\pi - \omega)}{\sin \eta(\pi - \omega)} e^{i2\eta(\pi - \omega)} - \right.$$

$$\left. - \sin \eta\omega \frac{(\eta - 1)(\pi - \omega)}{\sin (\eta - 1)(\pi - \omega)} e^{i2\eta(\pi - \omega) - i2\omega} \right\}$$

and putting into (III, 3) we can finally obtain the components of force on the cylinder.