

Partial Discharge Inception Characteristics under Butt Gap Condition in Liquid Nitrogen/PPLP[®] Composite Insulation System for High Temperature Superconducting Cable

M. Hazeyama, T. Kobayashi, N. Hayakawa

Department of Electrical Engineering
Nagoya University, Furo-cho, Chikusa-ku
Nagoya, 464-8603 Japan

S. Honjo

Tokyo Electric Power Company, Yokohama, Japan

T. Masuda

Sumitomo Electric Industries Ltd., Osaka, Japan

and H. Okubo

Department of Electrical Engineering
Nagoya University, Nagoya, 464-8603 Japan

ABSTRACT

The partial discharge (PD) inception characteristics are studied in liquid nitrogen (LN₂)/polypropylene laminated paper (PPLP[®]) composite insulation system for high temperature superconducting (HTS) cable. Experimental results revealed that the magnitude of the initial PD increased as the PD inception electric field strength was increased, because the injected energy increased. Initial PD was generated at the first and third quadrant of applied ac voltage phase. The probability of initial PD at the positive and negative voltage phase was almost the same. The reason is because liquid nitrogen is nonpolar molecule and we used symmetric electrode configuration with uniform electric field distribution. Finally, it was pointed out that PD inception electric field strength (PDIE) depended on the volume of the butt gap because of the increasing probability of weak points of electrical insulation, and PDIE linearly decreased with increasing stressed volume of the butt gap in the log-log scale.

1 INTRODUCTION

IN the last ten years, HTS power cables cooling by LN₂ has been increasingly used worldwide [1–4]. In the HTS cable, it is crucial to clarify the partial discharge (PD) inception mechanism in liquid nitrogen/PPLP[®] composite insulation system. Especially, butt gaps existing in the laminated insulation tapes should be taken into account, because PD may be generated in the butt gap and directly affect the electrical insulation performance [5–9]. Although, volume effects in the breakdown strength in LN₂ have intensely been studied, little is known about PD inception characteristics as influenced by the butt gap volume in LN₂/solid insulation system for HTS power cables [10].

In this paper, we report on the PD inception characteristics as influenced by the volume of the butt gap in liquid nitrogen/PPLP[®] composite insulation for HTS cable. Especially, we investigated the PD inception characteristics dependence on the number of butt gaps.

2 EXPERIMENTAL

Figure 1 shows the structure of HTS cable developed by Tokyo Electric Power Company and Sumitomo Electric Industries, Ltd. [1]. In Figure 1, for the electrical insulation of HTS cable, PPLP[®] impregnated with liquid nitrogen LN₂ is used because of the high properties of high insulation strength and low dielectric loss. By taking the electrical insulation layer of the HTS cable as shown in Figure 1 into account, we have made the electrode configuration of LN₂/PPLP[®] composite insulation system,

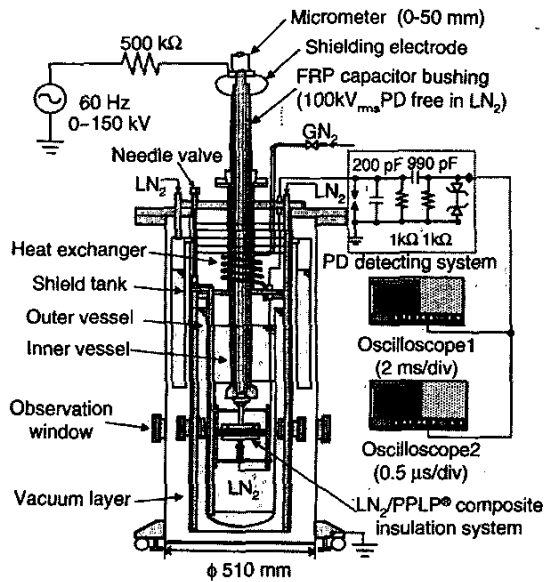
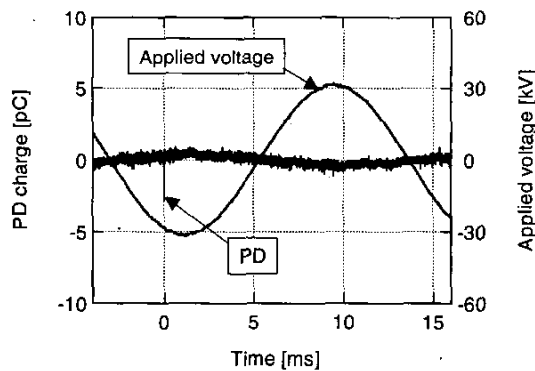
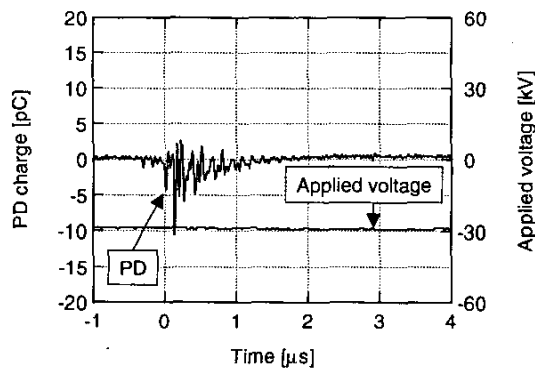


Figure 4. Experimental setup.



(a) Voltage phase characteristics of PD.



(b) Waveform of first PD.

Figure 5. PD inception characteristics of 3-layer PPLP® system at SLV = 30.9 mm³. Applied voltage, $V_{ac} = 22.0$ kV_{rms}; a, Voltage phase characteristics of PD; b, Waveform of first PD.

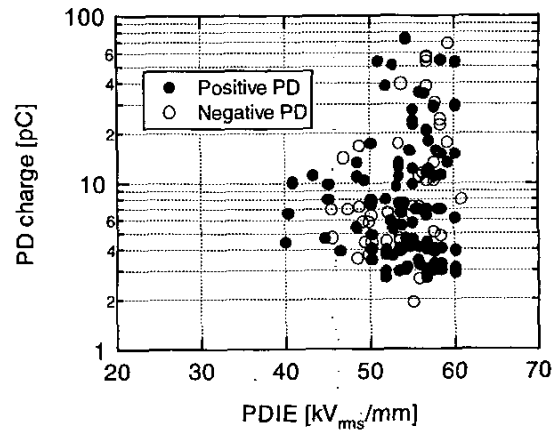
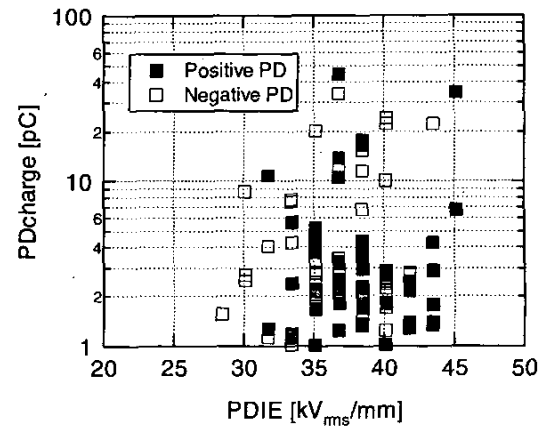
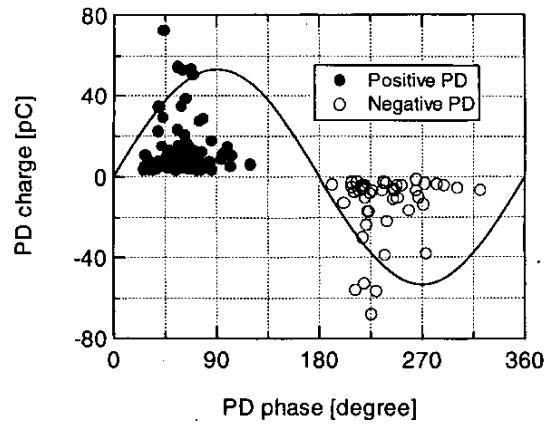
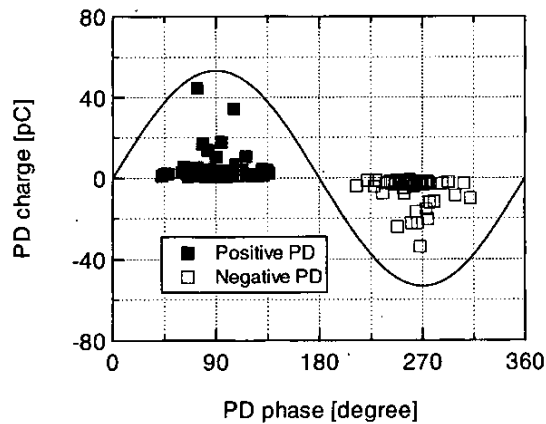
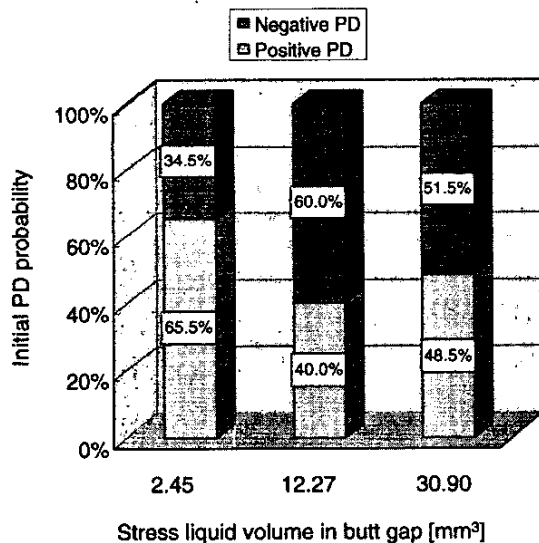
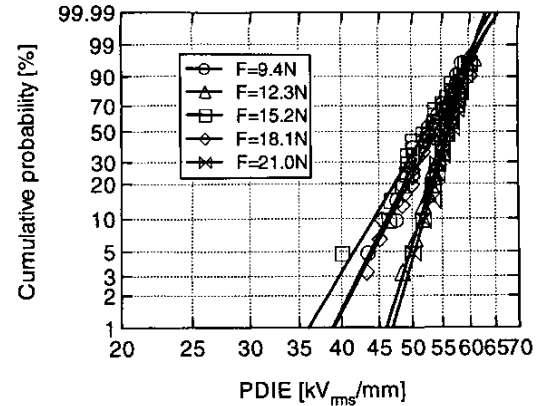
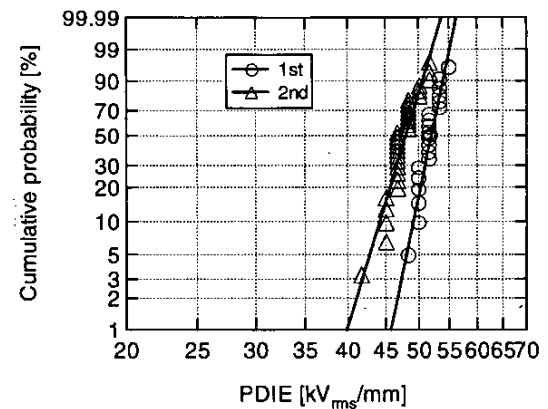
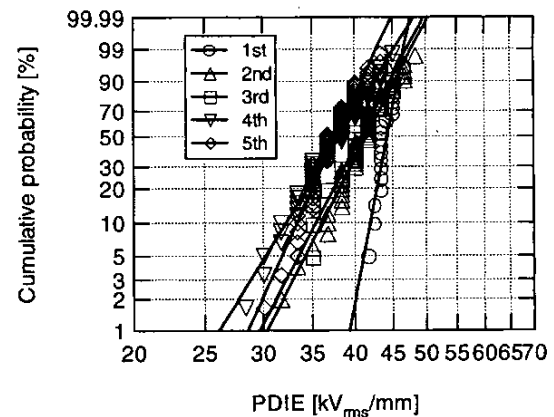
(a) SLV = 2.45 mm³(b) SLV = 30.90 mm³

Figure 6. PD charge as a function of PDIE. a, SLV = 2.45 mm³; b, SLV = 30.90 mm³.

4 ELECTRIC FIELD STRENGTH OF PD INCEPTION IN BUTT GAP

Figure 8 shows the initial PD generation probability at positive and negative polarity for different SLV in a butt gap. Figure 8 indicates that the initial PD polarity is independent of the different SLV because of symmetric electrode configuration with a uniform electric field distribution. From Figure 8, it can be said that the factor of generated PD would be the same because PD is always generated in the butt gap for different SLV.

Figure 9 shows typical Weibull plots of PDIE in butt gaps for (a) SLV = 2.45 mm³, (b) SLV = 12.27 mm³ and (c) SLV = 30.9 mm³. In these figures, F is the mechanical pressure of PPLP® surface. A reproducibility of PDIE data was confirmed by twice and five times measurements at SLV = 12.27 mm³ and SLV = 30.9 mm³ in Figure 9 (b) and (c), respectively. As indicated in these figures, PDIE

(a) $SLV=2.45 \text{ mm}^3$ (b) $SLV=30.90 \text{ mm}^3$ **Figure 7.** Voltage phase characteristics of initial PD. a, $SLV = 2.45 \text{ mm}^3$; b, $SLV = 30.9 \text{ mm}^3$.**Figure 8.** Initial PD generation probability at positive and negative polarity for different SLV.(a) $SLV=2.45 \text{ mm}^3$ (b) $SLV=12.27 \text{ mm}^3$ at $F=4.9 \text{ N}$ (c) $SLV=30.90 \text{ mm}^3$ at $F=4.9 \text{ N}$ **Figure 9.** Weibull plots of PDIE for different butt gap condition. a, $SLV = 2.45 \text{ mm}^3$; b, $SLV = 12.27 \text{ mm}^3$ at $F = 4.9 \text{ N}$; c, $SLV = 30.9 \text{ mm}^3$ at $F = 4.9 \text{ N}$.

characteristics follow the Weibull distribution and 50% cumulative probability of PDIE ($PDIE_{50}$) is decreased as SLV is increased. We calculate $PDIE_{50}$ and the shape parameter of m_e of PDIE from the Weibull distribution to discuss PD inception characteristics in detail.

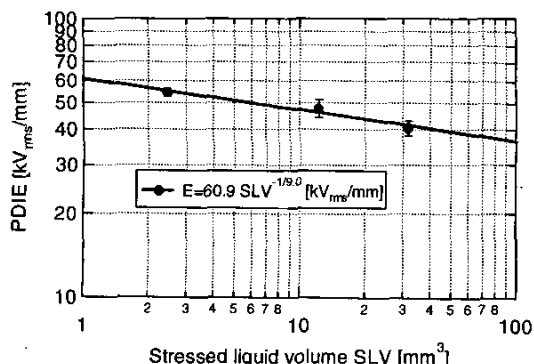


Figure 10. PDIE as a function of SLV in 3-layer PPLP® system.

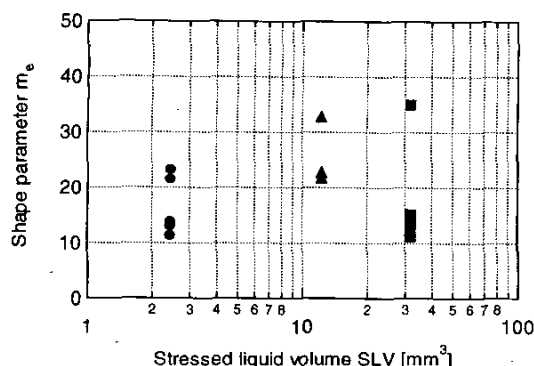


Figure 11. Shape parameter m_e as a function of SLV in 3-layer PPLP® system.

Figures 10 and 11 show $PDIE_{50}$ and m_e for different SLV in a butt gap for 3-layer PPLP® system. In Figure 11, the shape parameter m_e means the dispersion of PDIE and m_e in Weibull distribution is larger as the dispersion of PDIE is smaller. In Figure 10, $PDIE_{50}$ linearly decreases along with the volume of butt gaps in the log-log scale. Approximated equation is obtained as follow,

$$E = 60.9SLV^{-1/9.0} \quad [kV_{rms}/mm] \quad (1)$$

The volume effect of PDIE must be taken into account in the insulation design of actual HTS power cables.

Let us discuss the experimental results from the shape parameter of PDIE for different SLV in butt gap. From Figure 11, m_e at $SLV = 12.27 \text{ mm}^3$ is the largest for three different SLV. The two combined reasons might be considered: one reason is that as the volume of butt gap is increased, the weak points of electrical insulation performance are increased. The other one is that as the butt gap volume increases, PDIE decreases and then the shape parameter m_e decreases because the shape parameter depends on the magnitude of PDIE. Therefore, it can be

said that shape parameter m_e at $SLV = 12.27 \text{ mm}^3$ becomes the largest from this experiment.

5 CONCLUSION

IN this paper, we investigated PD inception characteristics in LN_2 /PPLP composite insulation system for HTS cable. Especially, we examined PD inception electric field strength as influenced by the volume of the butt gap. The main results are summarized as follows:

- (1) The initial PD charge is in the range 1–60 pC. The charges at smaller volume show slightly higher values.
- (2) The PD charge tends to be larger as PDIE increases at all butt gap conditions. The reason is that as PDIE increases, the injected energy which depends on the electric field strength in the butt gap is increased.
- (3) The voltage phase of the initial PD generation is independent of the butt gap condition. Almost all PDs are generated at the first and third quadrant of the ac voltage phase. The degree of the initial PD is shifted to the region around 90° at positive PD and 270° at negative PD, as SLV is increased.
- (4) The PD generating polarity is independent of SLV. $PDIE_{50}$ linearly decreases along with the volume of the butt gap in the log-log scale.
- (5) The shape parameter m_e at $SLV = 12.27 \text{ mm}^3$ is the largest for three different SLV. The reason is that firstly, as the volume of the butt gap is increased, the weak points of electrical insulation performance are increased, secondly as the butt gap volume increases, PDIE decreases and then the shape parameter m_e decreases because shape parameter depends on the magnitude of PDIE.

REFERENCES

- [1] S. Honjo, T. Mimura and Y. Takahashi, "Present Status of the Development of Superconducting Power Cable," *Physica C*, Vol. 335, pp. 11–14, 2000.
- [2] T. Masuda, T. Kato, Y. Ashibe, C. Suzawqa, M. Hirose, S. Isojima, S. Honjo, K. Matsuo, T. Mimura, T. Aina, and Y. Takahashi, "Development of a 100m-3core-114MVA HTSC cable system," 5th European Conference on Applied Superconductivity, Paper No. E4.1-05, 2001.
- [3] P. L. Ladie, M. Nassi, S. R. Norman, P. Caracino, M. Coevoet, C. Boisseau, and P. F. Sirot, "Pirelli-EDF Development on Superconducting Cables," *Proc. of Jicable*, pp. 103–108, 1999.
- [4] J. P. Stovall, J. A. Demko, P. W. Fisher, M. J. Gouge, J. W. Lue, U. K. Sinha, J. W. Armstrong, R. L. Hughey, D. Lindsay, and J. C. Tolbert, "Installation and Operation of the Southwire 30-meter High-Temperature Superconducting Power Cable," *IEEE Trans. on Applied Superconductivity*, Vol. 11, pp. 2467–2472, 2001.
- [5] J. Gerhold and T. Tanaka, "Cryogenic Electrical Insulation of Superconducting Power Transmission Lines: Transfer of Experience Learned From Metal Superconductors to High Critical Temperature Superconductors," *Cryogenics*, Vol. 38, pp. 1173–1188, 1998.
- [6] H. Okubo, M. Hikita, H. Goshima, H. Sakakibara and N. Hayakawa, "High Voltage Insulation Performance of Cryogenic Liquids for Superconducting Power Apparatus," *IEEE Trans. on Power Delivery*, Vol. 11, pp. 1400–1406, 1996.

- [7] A. Bulinski and J. Densley, "High Voltage Insulation for Power Cables Utilizing High Temperature Superconductivity", IEEE Electrical Insulation Magazine, Vol. 15, No. 2, pp. 14-22, 1999.
- [8] H. Suzuki, K. Ishihara, and S. Akita, "Dielectric Insulation Characteristics of Liquid-Nitrogen-Impregnated Laminated Paper-Insulated Cable", IEEE Trans. on Power Delivery, Vol. 7, pp. 1677-1680, 1992.
- [9] G. M. Hathaway, A. E. Davies, and S. G. Swinger, "Dielectric Considerations for a Superconducting Cable Termination", 11th International Symposium of High Voltage Engineering, Vol. 4, No. 467, pp. 84-87, 1999.
- [10] M. Hazeyama, N. Hayakawa, K. Matsuo, T. Masuda, and H. Okubo, "V-t Characteristics for Partial Discharge Inception of High Temperature Superconducting Power Cables", 5th European Conference on Applied Superconductivity, Paper No. E4.1-02, 2001.